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Thermodynamic implications on turbines of hydrogen fired turbofan engines

Kennis als Vermogen

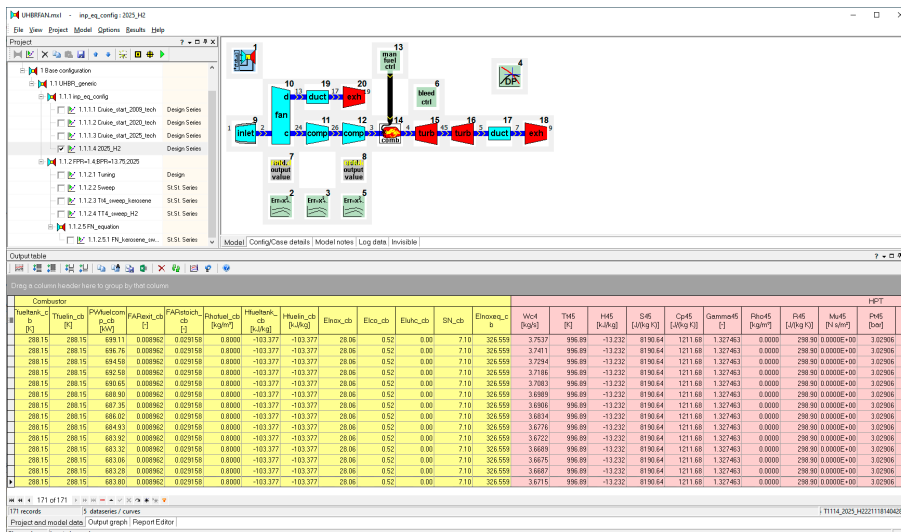


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Problem area

Reduced emission goals drive the research for using alternative aviation fuels. Hydrogen is an alternative fuel that is a candidate to be used in aviation (due to the volume, liquid hydrogen is considered a solution for aircraft fuel). The thermodynamic implications have not been well investigated or reported. This study will look into the thermodynamic loading of gas turbines design for hydrogen as well as retrofitting existing hydrocarbon jet fuel designs to be fuelled by hydrogen. Efficient Ultra-High Bypass Ratio (UHBR) turbofan engines having a high propulsive efficiency are used in this study.

Description of work

A generic UHBR turbofan model for NLR's Gas turbine Simulation Program, GSP, (from a previous study in determining the most efficient combination of fan pressure ratio, FPR, and bypass ratio, BPR) is used to calculate various hydrogen and hydrocarbon turbofan designs. An slightly adapted version of the model is used for simulating a retrofit turbofan engine that uses hydrogen as fuel while being designed to run on hydrocarbon jet fuel.

Results and conclusions

The simulations show that the optimum design point for a hydrogen design is different (optimum at higher BPR (ByPass Ratio) for given FPR (Fan Pressure Ratio)) than hydrocarbon jet fuel design running on pure hydrogen. The low pressure turbine (LPT) entry and exit temperature are higher for equivalent FPR and BPR values compared to the hydrocarbon jet fuel designs. For a retrofit gas turbine fuelled by hydrogen, the combustor temperature is lower compared to hydrocarbon jet fuel for equivalent thrust performance. For equivalent combustor exit temperature performance, the turbofan spool speeds are higher and may exceed design limits to negatively impact life expectancy. In the retrofit UHBR turbofan, the LPT entry and exit temperature are lower when fuelled by hydrogen compared to hydrocarbon jet fuel, while respecting all engine limits.

It is concluded that pure hydrogen UHBR designs will differ from the current hydrocarbon jet fuel designs as the core has a higher energy density, the optimum BPR is therefore higher for a given FPR. A higher average low pressure turbine temperature is foreseen which may implicate alternative designs (e.g. more cooling or different materials or coatings) to respect current life limits.

Modifying an existing turbofan engine to be fuelled by hydrogen would be possible as the thrust performance can be met at lower combustor exit temperatures while an increase in the life expectancy of the LPT is expected as the average operating temperature is lower compared to hydrocarbon jet fuel.

Applicability

This study gives insight into the implications of using hydrogen designed or hydrogen retrofitted turbofan engines. The results are interesting for after-market component developers that design and sell turbine related components like e.g. seals and blades.

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NLR

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Summary

Hydrogen is considered to be a sustainable alternative aviation fuel (when produced from renewable energy sources) for the future as an alternative to kerosene (hydrocarbon) jet fuel. However, hydrogen, either liquid or compressed is quite a different fuel with different fuel properties. The thermodynamic implications on turbines for commercial turbofans is investigated in this report using Ultra-High Bypass Ratio (UHBR) turbofan engines.

NLR's Gas turbine Simulation Program (GSP) is perfectly capable to simulate effects of using alternative fuels on new and existing design turbofan engines. The main reasons for this are that the GSP real gas model is derived from the NASA CEA (Chemical Equilibrium and Applications) model and offers the capability of using user-defined fuels. The different fuel properties cause a different thermodynamic profile which requires explorative calculations in GSP with hydrogen as fuel to gain understanding, insight and trust in the calculated results.

The thermodynamic implications in this study are focussed on the turbines when using hydrogen as fuel for a gas turbine designed for hydrogen or for an existing gas turbine designed for kerosene (retrofitting). It should be noted that when retrofitting existing engines for hydrogen, the fuel injection system and the combustor have to be modified.

A generic, configurable GSP gas turbine model of a UHBR turbofan is used for a hydrogen fuelled gas turbine design (exploration of fan pressure ratio, FPR, and bypass ratio, BPR) and a conventional hydrocarbon jet fuel design retrofitted to use hydrogen.

The simulations show that the optimum design point for a hydrogen design is different (optimum at higher BPR (ByPass Ratio) for given FPR (Fan Pressure Ratio)) than hydrocarbon jet fuel design running on pure hydrogen. The low pressure turbine (LPT) entry and exit temperature are higher for equivalent FPR and BPR values compared to the hydrocarbon jet fuel designs. For a retrofit gas turbine fuelled by hydrogen, the combustor temperature is lower compared to hydrocarbon jet fuel for equivalent thrust performance. For equivalent combustor exit temperature performance, the turbofan spool speeds (LP and HP) are higher and may exceed design limits thus negatively impact life expectancy. In the retrofit UHBR turbofan, the LPT entry and exit temperature are lower when fuelled by hydrogen compared to hydrocarbon jet fuel, while respecting all engine limits.

It is concluded that pure hydrogen UHBR designs will differ from the current hydrocarbon jet fuel designs as the core has a higher energy density, the optimum BPR is therefore higher for a given FPR. A higher average low pressure turbine temperature is foreseen which may implicate alternative LPT designs (e.g. more cooling or different materials or coatings) to respect current life limits.

Modifying an existing turbofan engine to be fuelled by hydrogen would be possible as the thrust performance can be met at lower combustor exit temperatures while an increase in the life expectancy of the LPT is expected as the average operating temperature is lower compared to hydrocarbon jet fuel.

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Abbreviations

ACRONYM	DESCRIPTION
3	Subscript used to denote compressor exit (combustor entry) station
4	Subscript used to denote combustor exit (HPT entry) station
45	Subscript used to denote HPT exit (LPT entry) station
5	Subscript used to denote LPT exit station
BPR	ByPass Ratio
DNW	German-Dutch Wind Tunnels
FPR	Fan Pressure Ratio
GSP	NLR's Gas turbine Simulation Program
HP	High Pressure
HPC	High Pressure Compressor
HPT	High Pressure Turbine (driving the HPC)
MTOW	Maximum Take-Off Weight
N%1	The fan (or low pressure) spool speed
N%2	The core (high pressure) spool speed
NLR	Royal NLR - Netherlands Aerospace Centre
NOx	Nitrogen Oxides emissions
LP	Low Pressure
LPT	Low Pressure Turbine (driving the fan)
OPR	Overall Pressure Ratio
TOC	Top Of Climb
TSFC	Thrust Specific Fuel Consumption
Tt#	Total/Stagnation Temperature for station #
UHBR	Ultra-High Bypass Ratio

1 Introduction

The reduction of fuel burn to reduce carbon footprint requires exploration of different engine layouts. One such path is the increase of the fan bypass ratio (BPR) to lower the thrust specific fuel consumption (TSFC) by increasing the propulsive efficiency (see Figure 1). Large values of BPR (> 12) refer to Ultra-High Bypass Ratio engines (or UHBR engines). Optimising the engine layout for increased BPR requires altering other design parameters like changing the fan pressure ratio, the overall pressure ratio (OPR) and the combustor exit temperature (or high pressure turbine entry temperature Tt_4), cooling technology and component efficiencies.

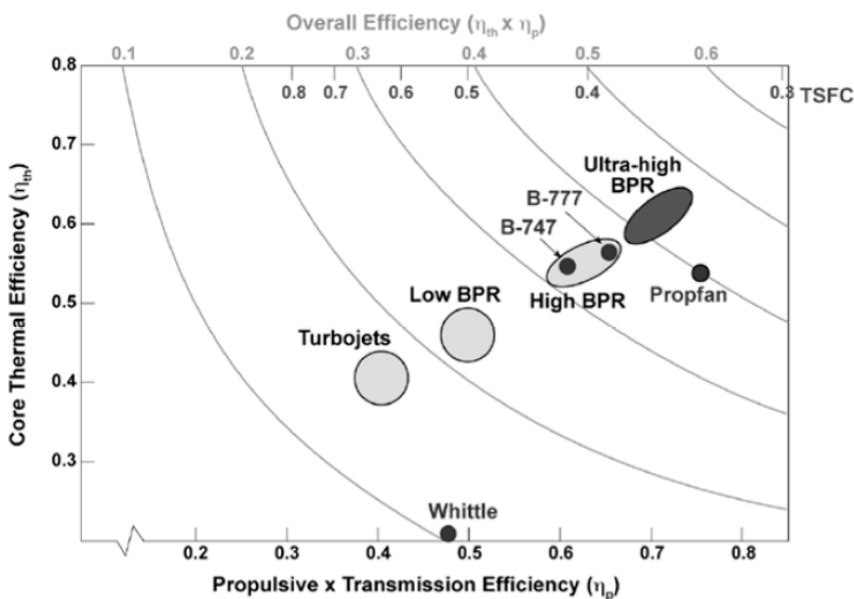


Figure 1 - The link of SFC and overall efficiency with thermal efficiency and propulsive efficiency [ref. Epstein]

Hydrogen is considered to be a sustainable alternative aviation fuel for the future as an alternative to kerosene reducing the carbon footprint further (although hydrogen doesn't contain carbon, it is possible that it may have been used in the production or transportation, this study focusses on the use of the fuel in the aircraft). However, hydrogen, either liquid or compressed is quite a different fuel with different fuel properties (e.g. specific volume, temperature of liquid state, heating value, etc.). The use of this fuel may have implications on turbine loading for commercial turbofans. This is investigated for the aforementioned Ultra-High Bypass Ratio (UHBR) turbofan engine.

NLR's Gas turbine Simulation Program (GSP) is perfectly capable to simulate effects of using alternative fuels on new and existing design turbofan engines. The main reasons for this are that the GSP real gas model is derived from the NASA CEA (Chemical Equilibrium and Applications) model and offers the capability of using user-defined fuels. Note that this study focusses on the thermodynamic effects on the turbine, the effects of the production of nitrogen oxides (NOx) is not considered as this is highly depending on the geometry of the combustor and the premixing of the fuel.

1.1 Engine model

This study uses a model (see Figure 2), developed with NLR’s Gas turbine Simulation Program, that is inspired by the study of Dr. Nicholas Cumpsty [ref. Cumpsty]. The generic UHBR model is intended to be used for calculating the specific fuel consumption based on varying:

- Fan bypass ratio (BPR)
- Fan pressure ratio (FPR)
- Overall cycle pressure ratio (OPR)
- Turbine entry temperature (Tt4)

The (start of the) cruise segment (or top of climb, TOC) is chosen for the analysis. A well-known condition for this reference point is 35,000 feet (10668 m) with a Mach number of 0.8 (these ambient conditions are used in this analysis unless otherwise specified). The engine thrust (net thrust is denoted as FN) range is chosen in the range to power a Boeing 787 having a take-off power of about 340 kN. For start of the cruise segment it implies that the thrust at start of the cruise segment roughly equals $FN_{cruise} = MTOW/21$ (Maximum Take-Off Weight divided by the optimum lift/drag ratio of 21).

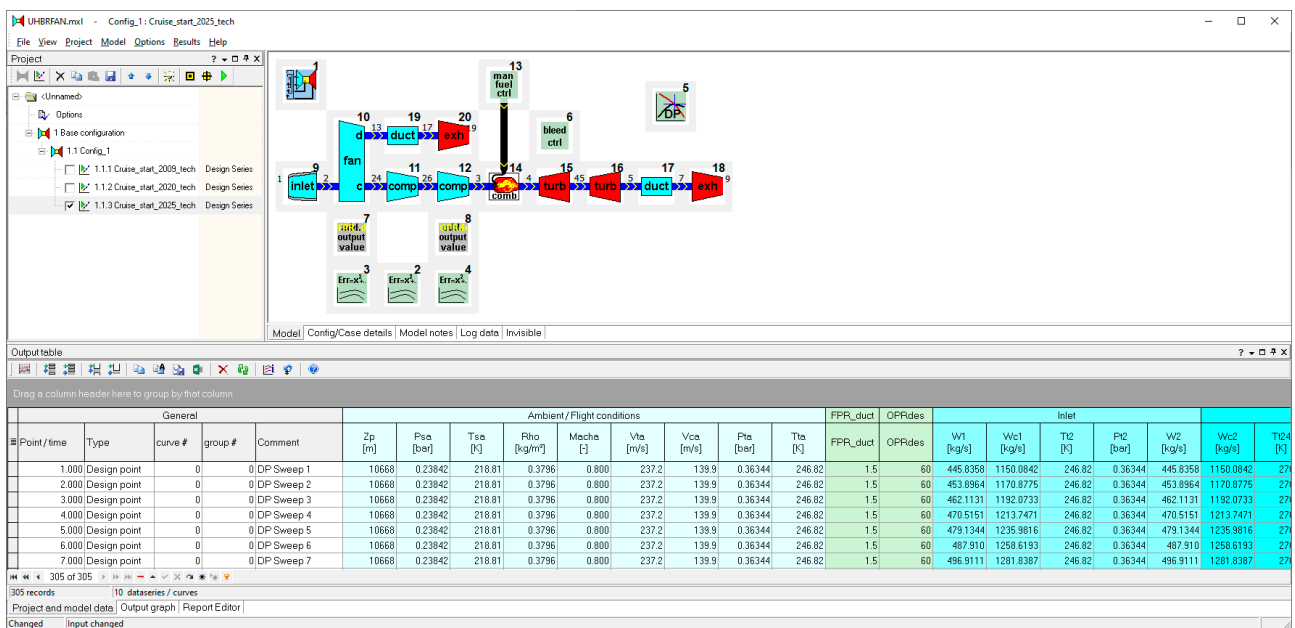


Figure 2 - Screenshot of the GSP UHBR turbofan model

The model (see Appendix A for a textual listings of the models) itself consists of some advanced modelling techniques to calculate various designs sequentially by the use of a case control input specification component (to specify series of design point operating points; this is component model marked with a Nr. 1 in the top right corner, see zoomed model in Figure 3). This series control component schedules the FPR_{duct} and the BPR . is FPR_{duct} set in component #7 (by case input controller #1) and this value is used in components #2 and #3 to set the values of core FPR ($0.95 * FPR_{duct}$) and duct FPR (FPR_{duct}) respectively in the fan module #10. Cooling bleed is scheduled using component #6 (the amount of cooling bleed is based on the maximum turbine inlet temperature; the better the cooling and material technology, the higher the allowable gas temperature and the higher the amount of cooling flow). Furthermore, component #8 defines the OPR of the cycle, from which component #4 sets the high pressure compressor (HPC) design pressure ratio. Furthermore, a design point iterator (component #5) has been added to iterate to a design inlet mass flow for a given design thrust value. The value for cruise thrust in this analysis is 54 kN.

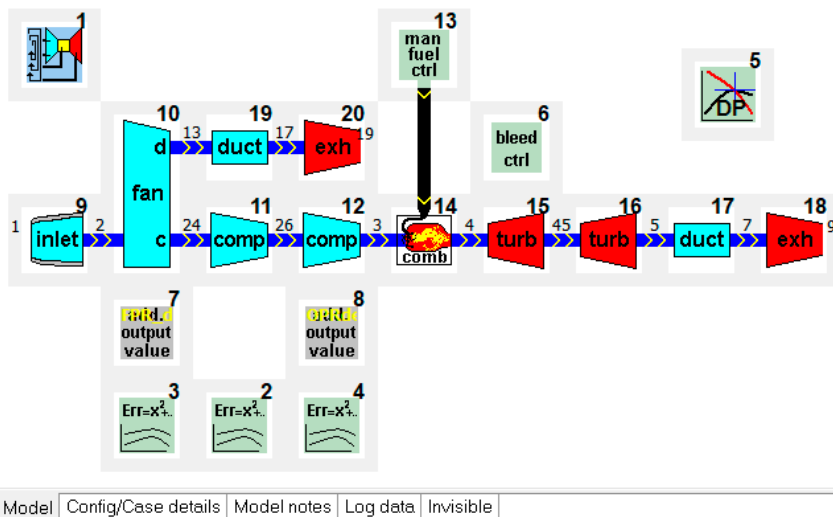


Figure 3 - Close-up of the model consisting of stacked component models

1.2 Hydrogen UHBR turbofan design

The first analysis (see chapter 2) will consider that the UHBR turbofan is developed/ designed to use hydrogen as fuel from scratch (complete new design). These results will be compared to kerosene fuelled UHBR turbofans for exactly the same performance. As design performance point, the end of top of climb will be used for the comparison; the reason for choosing this point is that this is the critical flight phase for the engine design. The resulting thermodynamic properties will be interpreted and compared.

1.3 Retrofitting existing UHBR turbofan

The second analysis (see chapter 3) will consider a kerosene designed UHBR turbofan that is retrofitted with a different combustor to allow using hydrogen as an alternative fuel. The performance at TOC is again considered and will be kept constant, if the engine stays within limits, otherwise the limits are respected. The resulting thermodynamic properties will be interpreted and compared to kerosene results.

2 Analysis of H2 fuelled UHBR turbofan designs

For the analysis of the thermodynamic implications on multiple spool engines, a UHBR turbofan engine with 2025 technology level has been chosen that has a thrust range to power a Boeing 787 (having a take-off power of about 340 kN). With an OPR of 60, a turbine inlet temperature of 1650 Kelvin and an amount of cooling flow of 25 %, we obtain the result as depicted in Figure 4. In this graph the FPR is varied from 1.5 down to 1.3 in steps of 0.05 (5 curves, 1.5 to 1.3 from left to right).

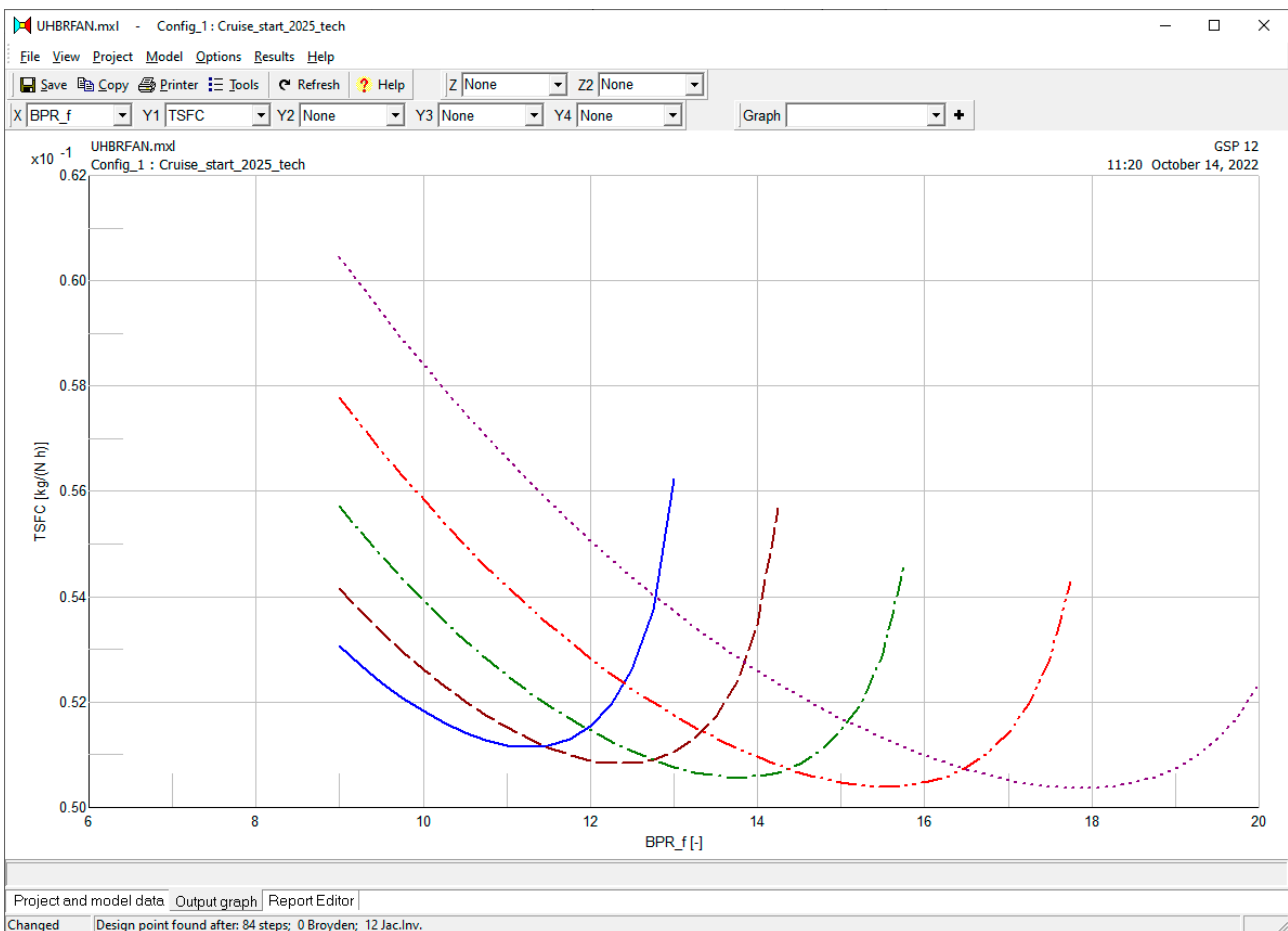


Figure 4 - Kerosene fuelled UHBR turbofan design sweep performance

A similar exercise has been performed for the hydrogen fuelled UHBR turbofan, see Figure 5. When combining the 2 figures (Figure 4 and Figure 5) we obtain Figure 6. From this figure we observe that the hydrogen fuelled turbofan results (bottom curves) have a lower thrust specific fuel consumption (TSFC) than the kerosene results (top curves). Furthermore, to show a minimum TSFC for hydrogen fuelled UHBR turbofans we had to increase the BPR to higher values. The minimum values of the hydrogen curves is further to the right than for kerosene. This implies that the core can be designed smaller for hydrogen fuel than for kerosene, hydrogen cores have a higher power to volume density.

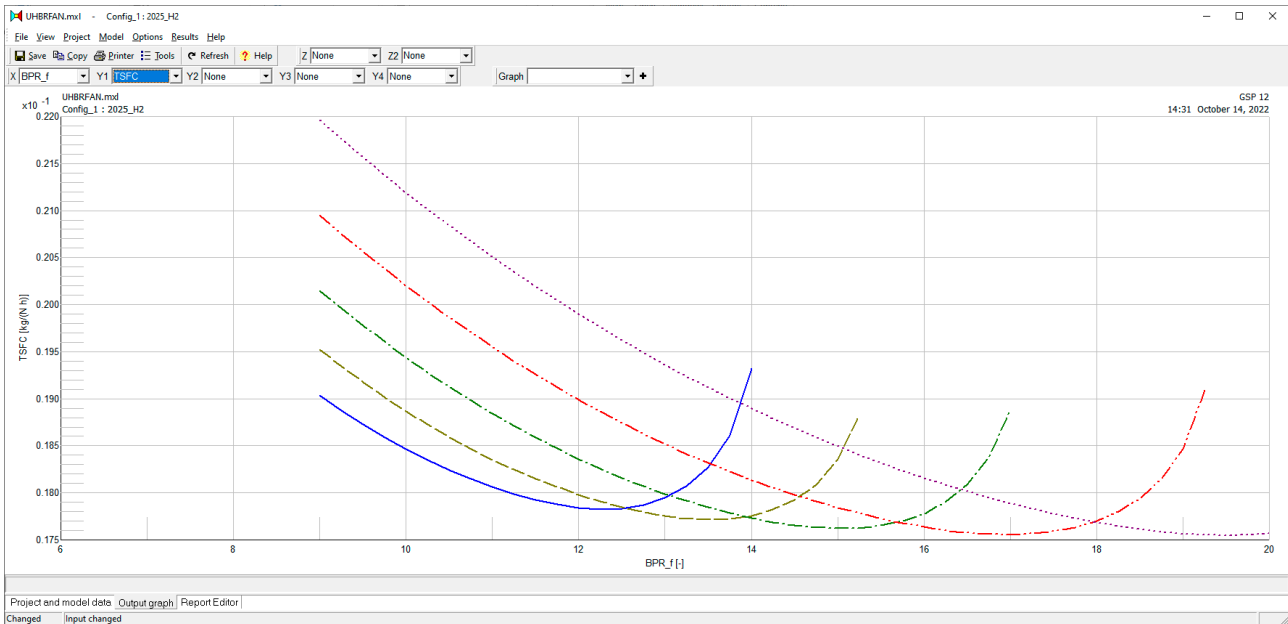


Figure 5 - Hydrogen fuelled UHBR turbofan design sweep performance

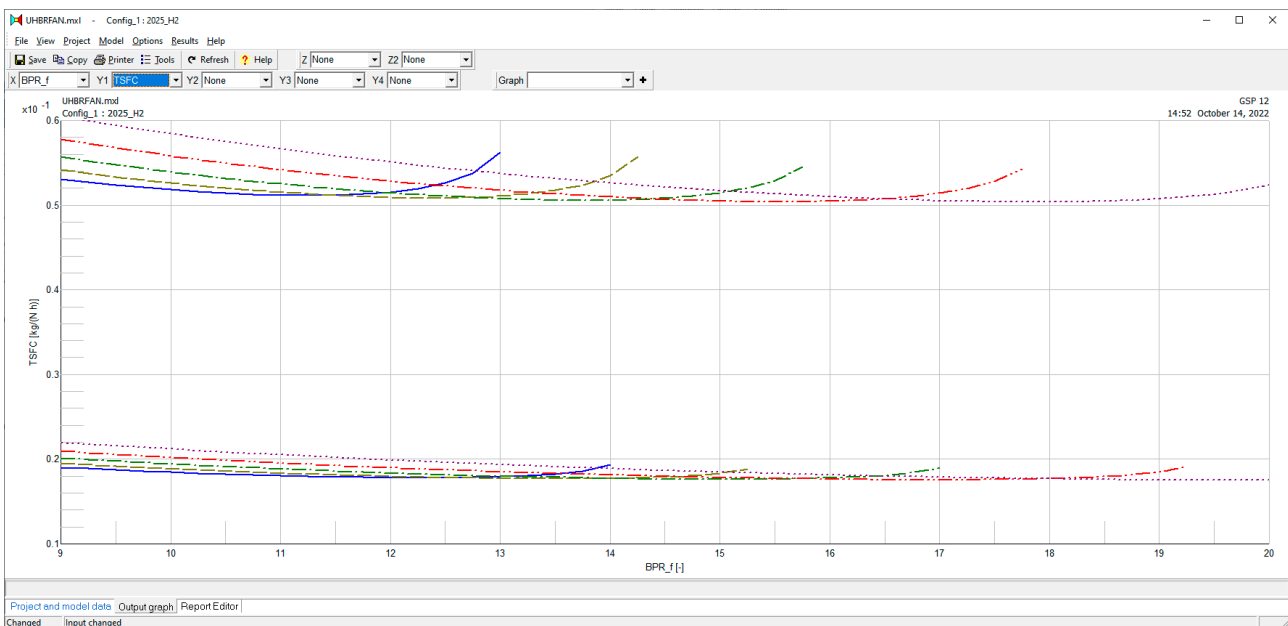


Figure 6 - Hydrogen (lower curves) and kerosene (top curves) fuelled UHBR turbofan design sweep performance

If we focus on the turbine thermodynamics of the UHBR turbofan engines we have to plot the temperatures of the high pressure turbine (HPT; drives the high pressure compressor, HPC) and the low pressure turbine (LPT; drives the fan and booster). Note that since we fixed the combustor exit temperature (per the technology level) the temperature of the exhaust gases entering the HPT is for kerosene and hydrogen exactly the same, so there is no need to plot this temperature known as $Tt4$. Instead, we will plot $Tt45$ (HPT exit temperature or LPT entry temperature) and the $Tt5$ (LPT exit temperature or exhaust nozzle entry temperature). This is shown in Figure 7.

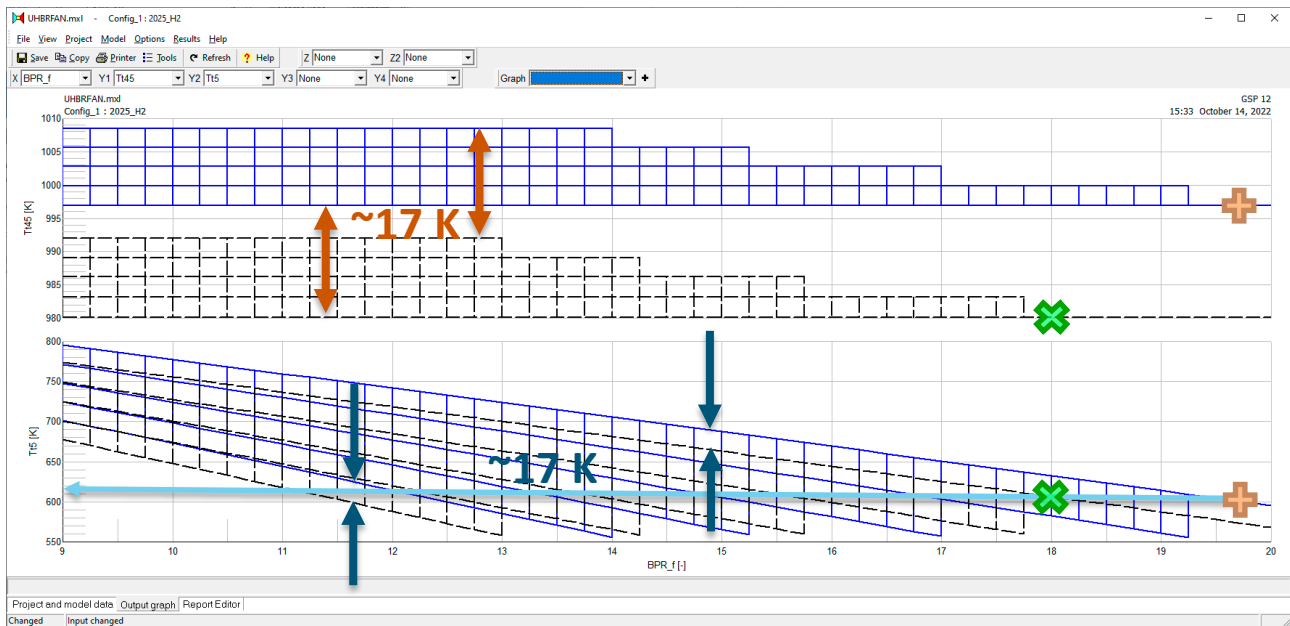


Figure 7 - UHBR turbofan turbine performance comparison (hydrocarbon jet fuel, black; hydrogen, blue)

Figure 7 shows the turbine temperatures for kerosene (black, dashed) and hydrogen (blue, solid). A remarkable observation from this figure is that the HPT exit temperature (Tt_{45}) for hydrogen fuelled turbofan engines is about 17 K higher than for kerosene fuelled UHBR turbofan engines. The LPT (Tt_5) exit temperature also is about 17 K higher. Note that this is a direct comparison for the same engines based on FPR and BPR. However, when we compare optimized designs (see for reference figures 4 and 5), e.g. the optimum design for a kerosene fuelled UHBR turbofan engine with an FPR value of 1.3 is found at a BPR value of 18 (green cross sign in Figure 7). For the same FPR, the optimum design for a hydrogen fuelled UHBR turbofan the BPR value is 19.5 (orange plus sign in Figure 7). The temperature difference for comparison of optimized designs remains at a value for ΔTt_{45} of 17 K (no change), and reduces for ΔTt_5 to a value of -2 K (in favour of hydrogen, this is caused by the distinct constant temperature profile of Tt_{45} and diverging profile Tt_5). This results in a higher average turbine temperature (from inlet to exit) which may have some implications on the life and the design of vanes and blades of the LPT.

3 Analysis of retrofitting a UHBR turbofan design

The previous chapter discussed the development of new designs that incorporate hydrogen as fuel from a design standpoint with the assumption of equivalent performance in terms of thrust compared to a kerosene fuel turbofan. This chapter will focus on retrofitting an existing design (designed for kerosene) to use hydrogen as an alternative fuel. Note that this requires changes to the combustor and fuel system, such changes are not applicable for this analysis as we will not consider them. The fuel will be fully burned. Taking combustor design into account would be of interest if the emissions of the turbofan would be analysed; emissions are excluded from this analysis, and hence, the configuration determined by the kerosene (hydrocarbon) jet fuel design can be used to combust hydrogen in off design (steady-state) analyses.

For this analysis a 2025 technology design for kerosene is chosen and used to run on hydrogen in steady state series off design analyses. An FPR of 1.4 and a BPR of 13.75 is chosen for the analysis. We understand that there are more efficient designs (for lower FPR and higher BPR). If the vast amount of effort and costs (when choosing a design with very low FPR and high BPR) to achieve only a small additional increase in overall efficiency is taken into account, such efforts do not justify the increase.

3.1 Flight envelope

The turbofan performance can be mapped from the flight envelope (Mach and Altitude) for various power settings. The chosen power setting for the simulation is combustor exit temperature, this is a technology limitation, which can be applied to both hydrocarbon jet fuel and hydrogen fuelled gas turbines.

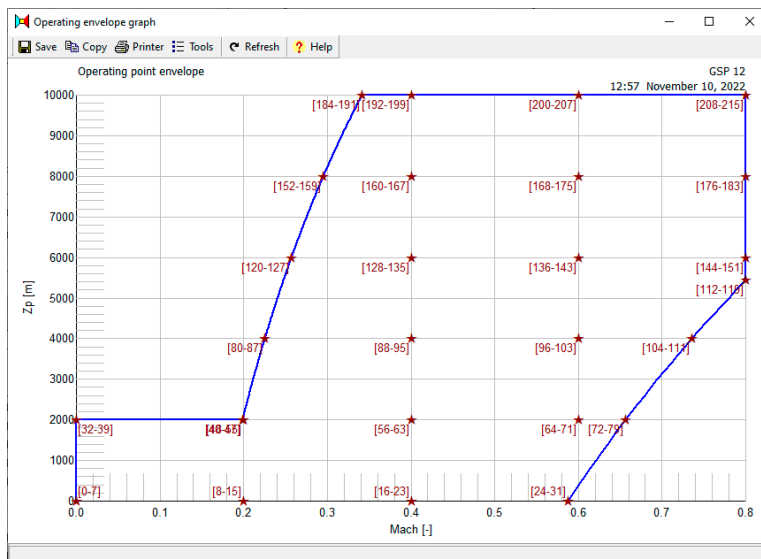


Figure 8 - Flight envelop

Figure 8 shows an example of the used flight envelop; the envelop cut-outs represent areas that are not actual flight conditions where engines cannot or don't have to provide thrust. The numbers in between square brackets represent the individual simulation number; this flight envelope contains 216 simulations (resulting in well over 1000 simulations as in between each simulation step 5 intermediate steps are used to prevent too large input deviations and thus iteration/non convergence issues).

3.2 UHBR turbofan simulations

Using a different fuel than the fuel the gas turbine is designed for should not affect the performance of the aircraft within the limitations of the engine (control) limits. Two types of analysis can be performed to ensure the performance of the engines is enough to power the aircraft:

1. Analysis respecting the gas turbine design limits, e.g. respecting combustor exit temperature, spool speeds.
2. Analysis calculating fuel requirement for aircraft performance, e.g. calculating the fuel flow or combustor exit temperature for the thrust specification of the aircraft in the flight envelope.

Both analyses yield results that can be used to evaluate if the change in fuel effects the gas turbine integrity or the flight performance. The second analysis requires changes to the UHBR model to calculate free state fuel flow/combustor exit temperature based on the input of a thrust requirement (this requires another equation in the model that generally requires more steps and thus longer simulation times apart from an extra step to generate input and modify the model). This is more complicated than the first type of analysis where the combustor exit temperature is maximized, so that the first type of analysis is explored first. For this analysis it is important to check the thrust generation after the simulation and other engine limits.

Running the various power ratings (maximum combustor exit temperature to a low temperature which corresponds to a high to low fuel flow value, but respecting the allowable material temperatures) for the various flight conditions (Mach or speed and altitude values) yields the thrust performance as depicted in Figure 9.

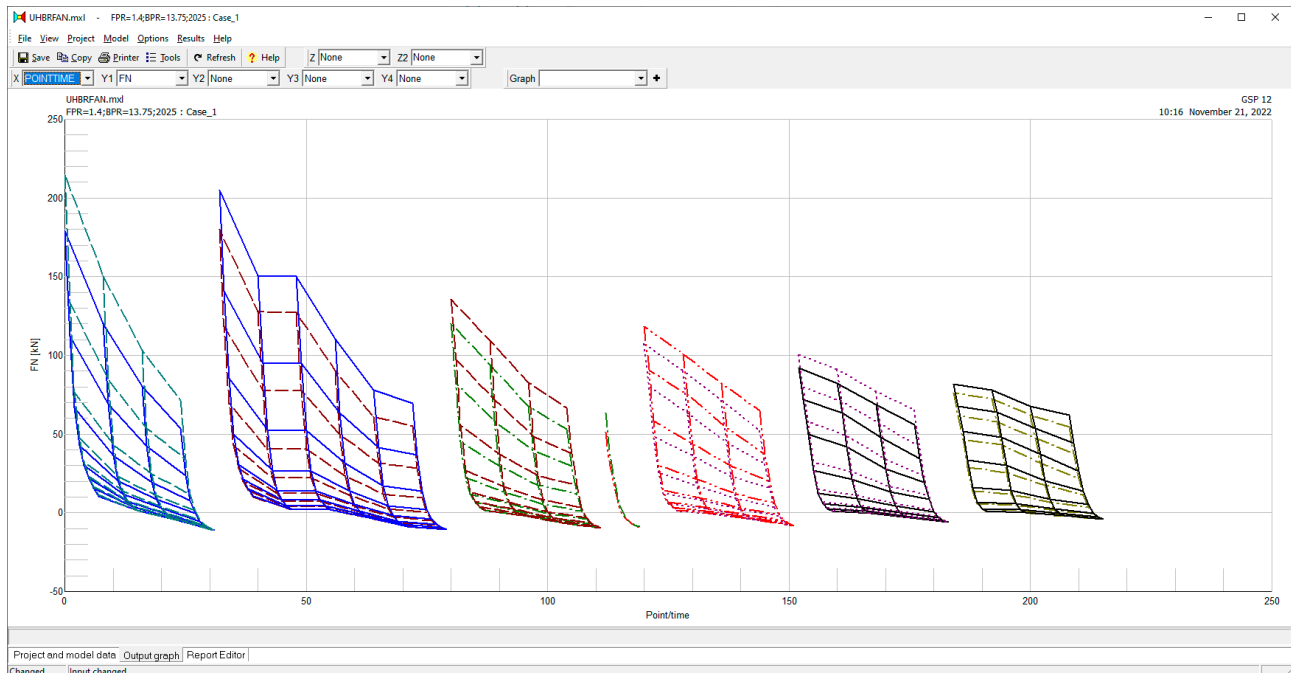


Figure 9 - Flight envelope performance for hydrocarbon jet fuel and Hydrogen

Figure 9 shows carpet plots for hydrocarbon jet fuel and Hydrogen fuel grouped by altitude as shown in Figure 8 (note that simulations 112-119 are a separate flight level) which may be a little difficult to read. Grouping the data for fuel type, we obtain Figure 10.

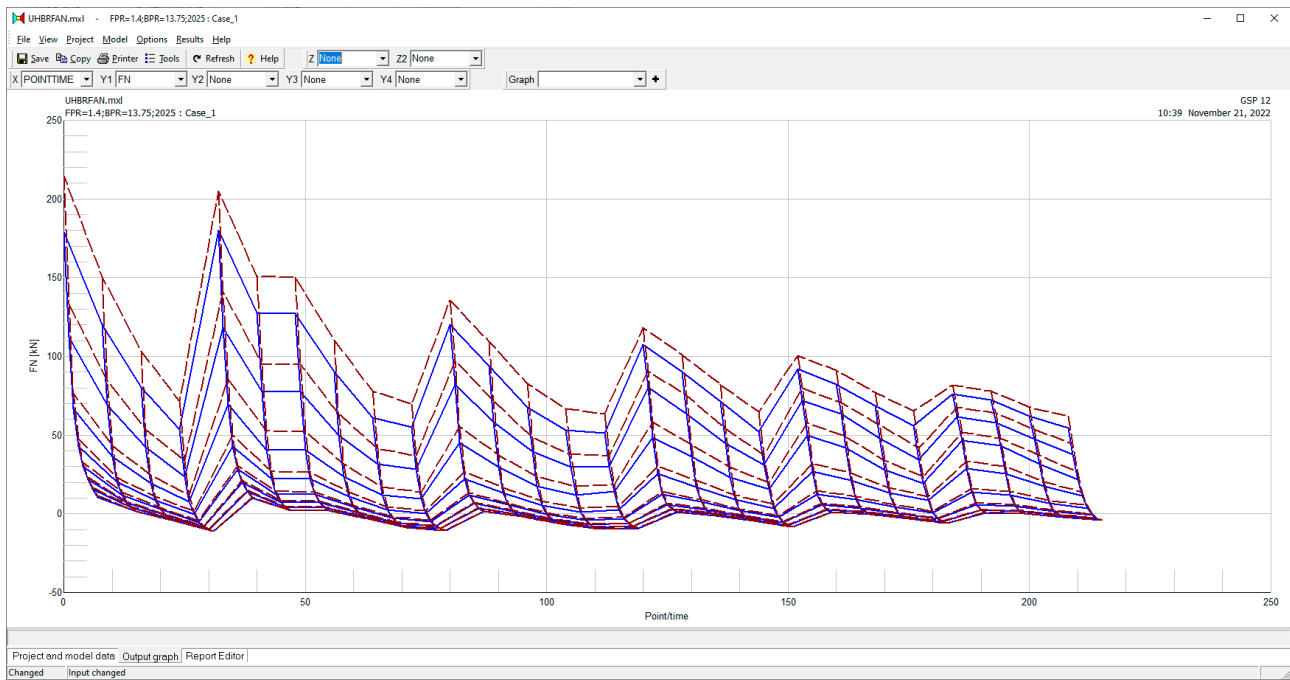


Figure 10 - Flight envelope thrust performance grouped by hydrocarbon jet fuel (solid blue) and Hydrogen (dashed brown)

The latter figure, grouped by fuel type shows that the thrust performance of Hydrogen fuel (dashed brown) surpasses the performance for hydrocarbon jet fuel (solid blue) while respecting the engine combustor exit temperature limits. This implies that enough thrust can be generated in a retrofit engine; it even implies that the temperature can be lowered to match the hydrocarbon jet fuel thrust performance. A lower temperature will cause components life to be extended. Other engine limits to check are spool speeds, see Figure 11 and HPC (high pressure compressor) exit pressure, Figure 12. High spool speeds cause high compressor exit pressure and increased stress levels in rotating parts like disks and rotor blades. The fan (or low pressure/LP) spool speed is denoted as N%1 and the core (high pressure/HP) spool speed is denoted as N%2 (see Figure 11).

Figures 11 and 12 show that when respecting the maximum allowable temperature of the combustor exit flow, the spool speeds and pressure exceed the values for hydrocarbon jet fuel. Whether this is acceptable depends on the construction of the compressor casing and the maximum allowable stress levels in rotating parts (blades and disks), but will certainly decrease component life. This implies that it is imperative to reduce the fuel flow when running on Hydrogen fuel (which should not be a problem since there is more thrust for the same combustor exit temperature).

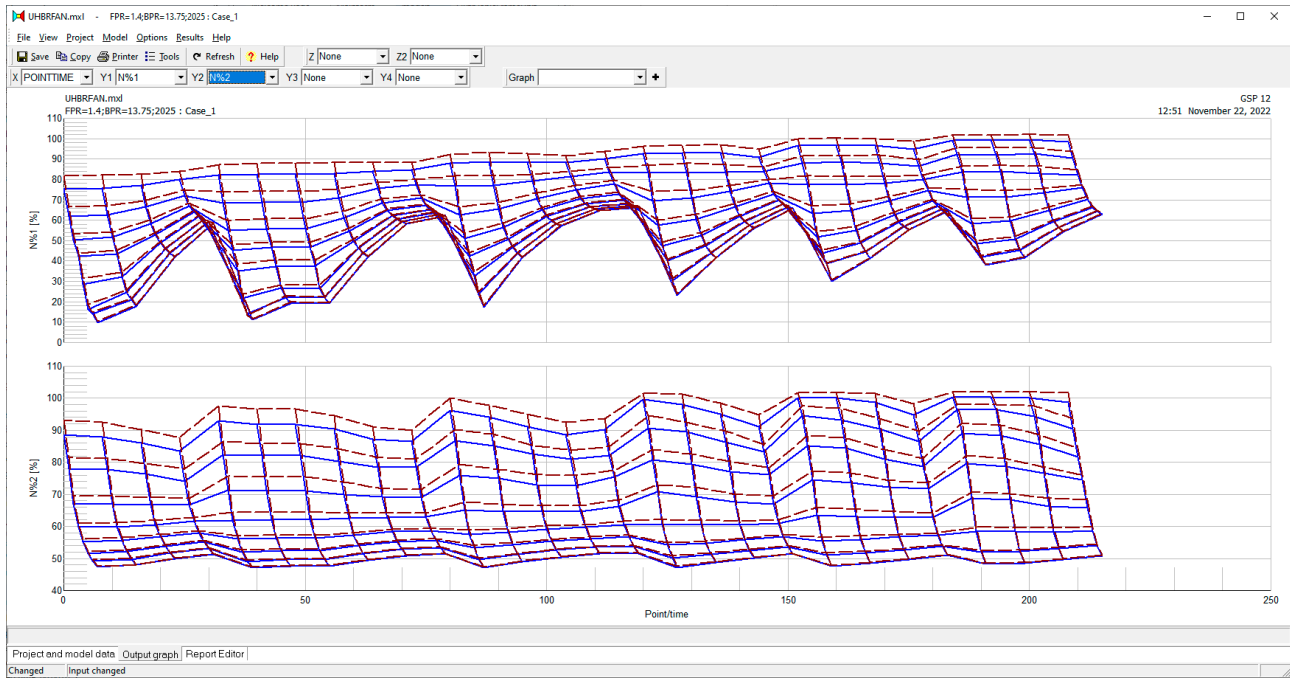


Figure 11 - Flight envelope spool speeds, hydrogen fuel (dashed, brown) hydrocarbon jet fuel (solid, blue)

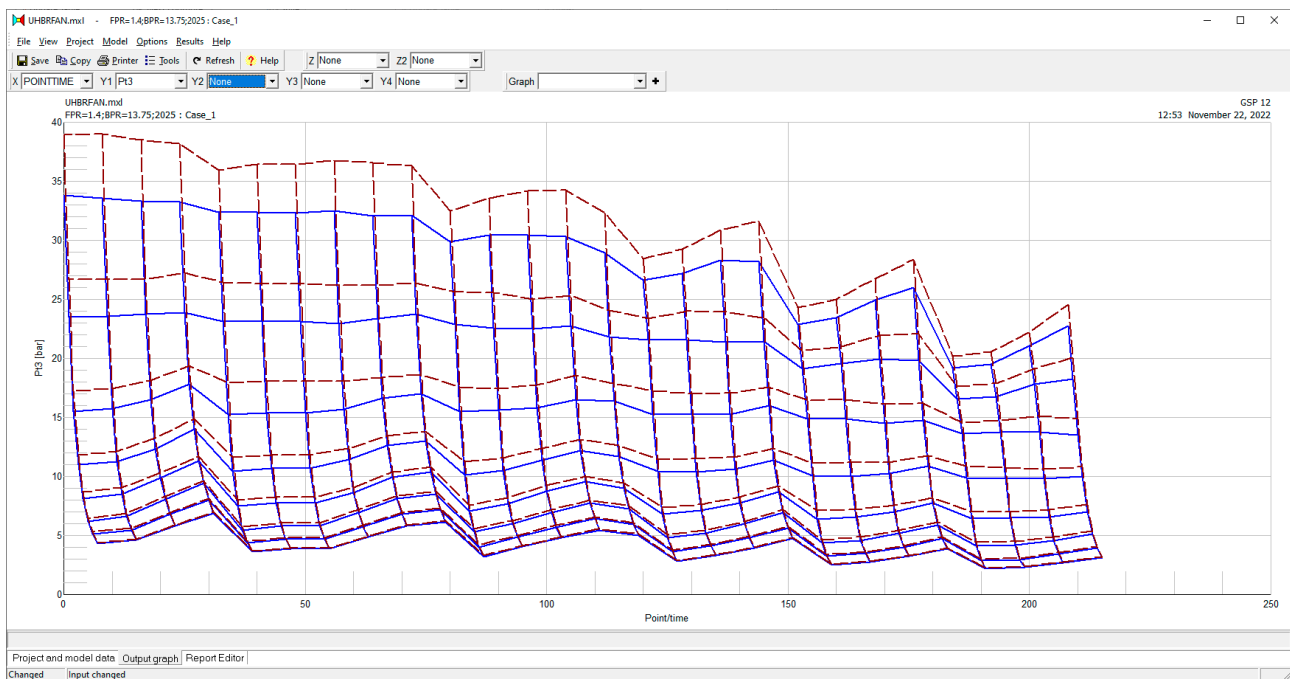


Figure 12 - Flight envelope compressor exit pressure, hydrogen fuel (dashed, brown) hydrocarbon jet fuel (solid, blue)

Further inspection of the low pressure turbine (LPT) inlet ($Tt45$) and exit ($Tt5$) temperature (see Figure 13) shows that the temperatures for hydrogen fuel (dashed, brown) are similar or lower than when running on hydrocarbon jet fuel (solid, blue).

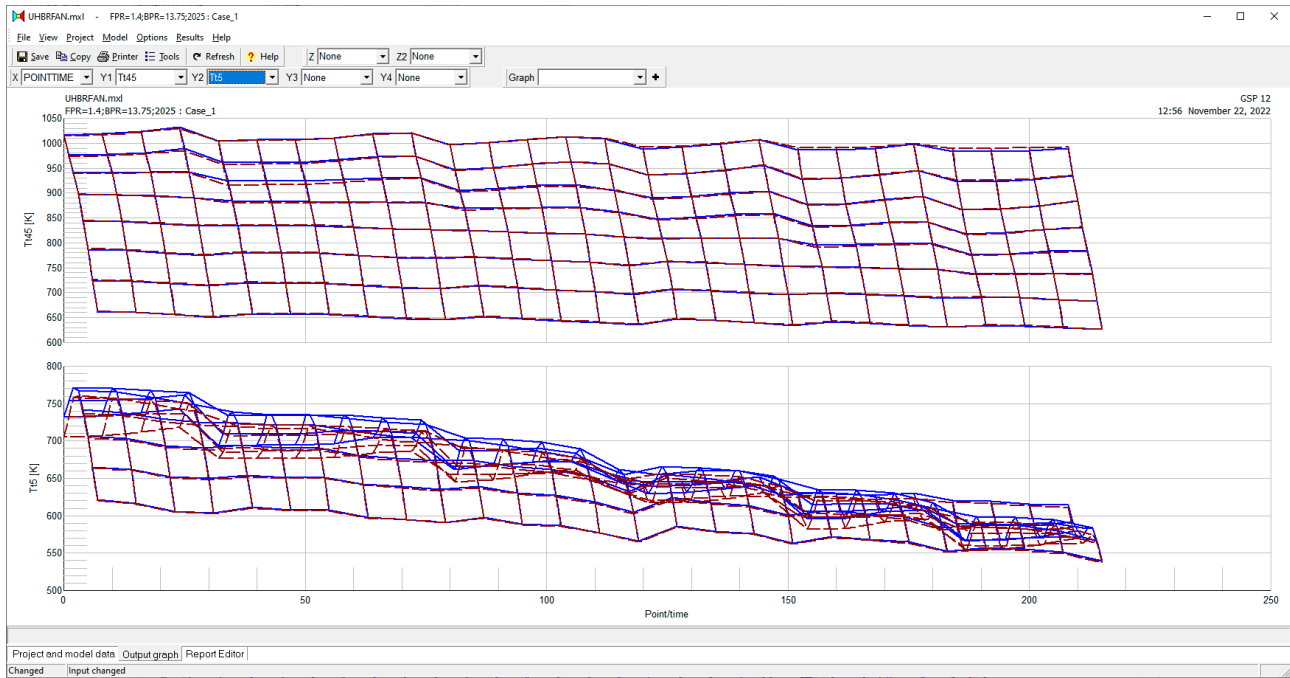


Figure 13 - Flight envelope LPT turbine temperatures, hydrogen fuel (dashed, brown) hydrocarbon jet fuel (solid, blue)

Now that several engine limits (spool speeds and HPC exit pressure) are exceeding the values while running on hydrogen with respect to the hydrocarbon jet fuel simulations, it would be best to check whether lowering the fuel flow (to lower the combustor exit temperature and as such lower spool speed and HPC exit pressure) alleviates the limit crossings when the same thrust performance is used for Hydrogen. We can now use the results generated for hydrocarbon jet fuel through a modification of the UHBR engine model by introducing an extra equation (Equation 1) and a free state variable (fuel flow).

$$(FN_{sim})_{v,alt} - (FN_{hc})_{v,alt} = 0 \quad (\text{Equation 1})$$

With this addition to the model, the calculated thrust performance (FN_{sim}) is compared to the previous calculated input value for hydrocarbon jet fuel (hydrocarbon thrust, FN_{hc}) for the same flight performance point (flight speed and altitude). The fuel flow is the independent free variable and is perturbed until the resulting error is within the error margin (nearly zero). Simulation convergence for low power settings (low to negative thrust values) is difficult to achieve, therefore, the bottom values of the calculated dataset for equal thrust performance (apple green, dashed line in e.g. Figure 14) are not always present and distort the carpet plot at the bottom of the figures, please ignore this in figures 14 to 17. As can be seen in Figure 14, the net thrust for running on hydrogen equals the net thrust for running on kerosene (except for the low power settings due to convergence issues).

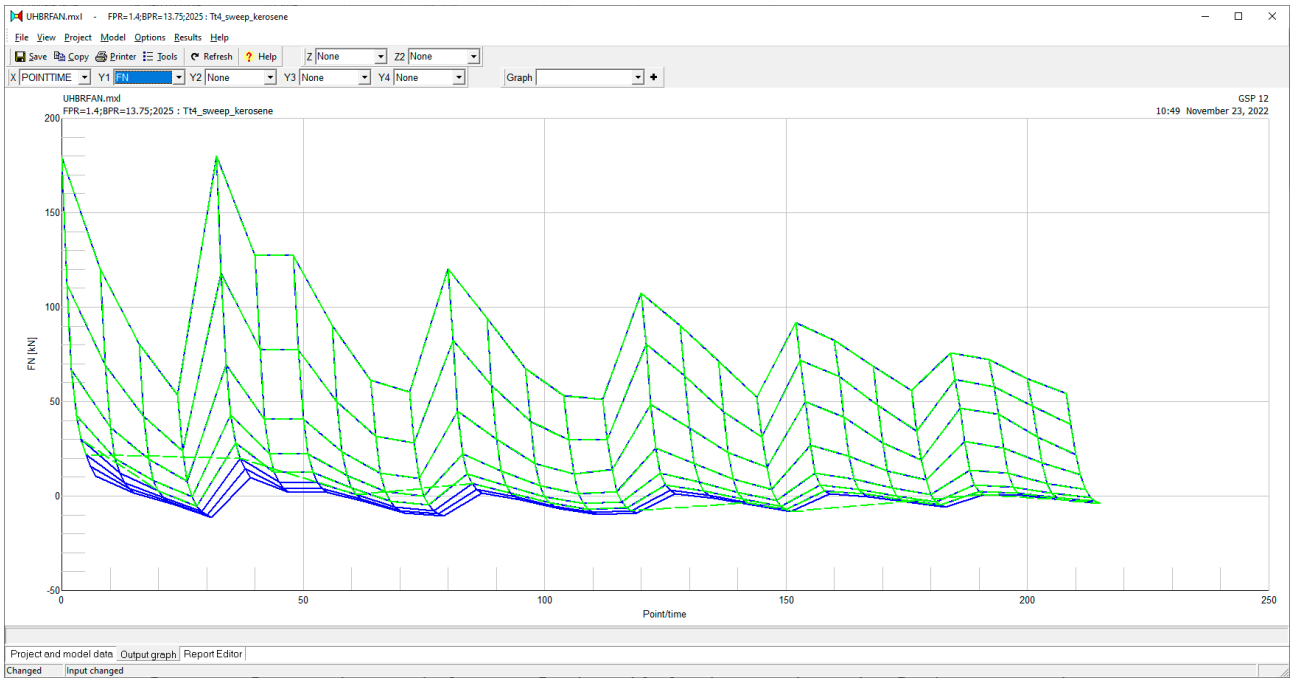


Figure 14 - Flight envelope thrust performance grouped by fuel type, hydrocarbon (solid blue) and hydrogen (dashed green)

The engine limitations for spool speed and HPC exit pressure to confirm the compressor exit pressure drop are revisited in figures 15 and 16. From these figures we see that the limits are respected, the values are equivalent or lower.

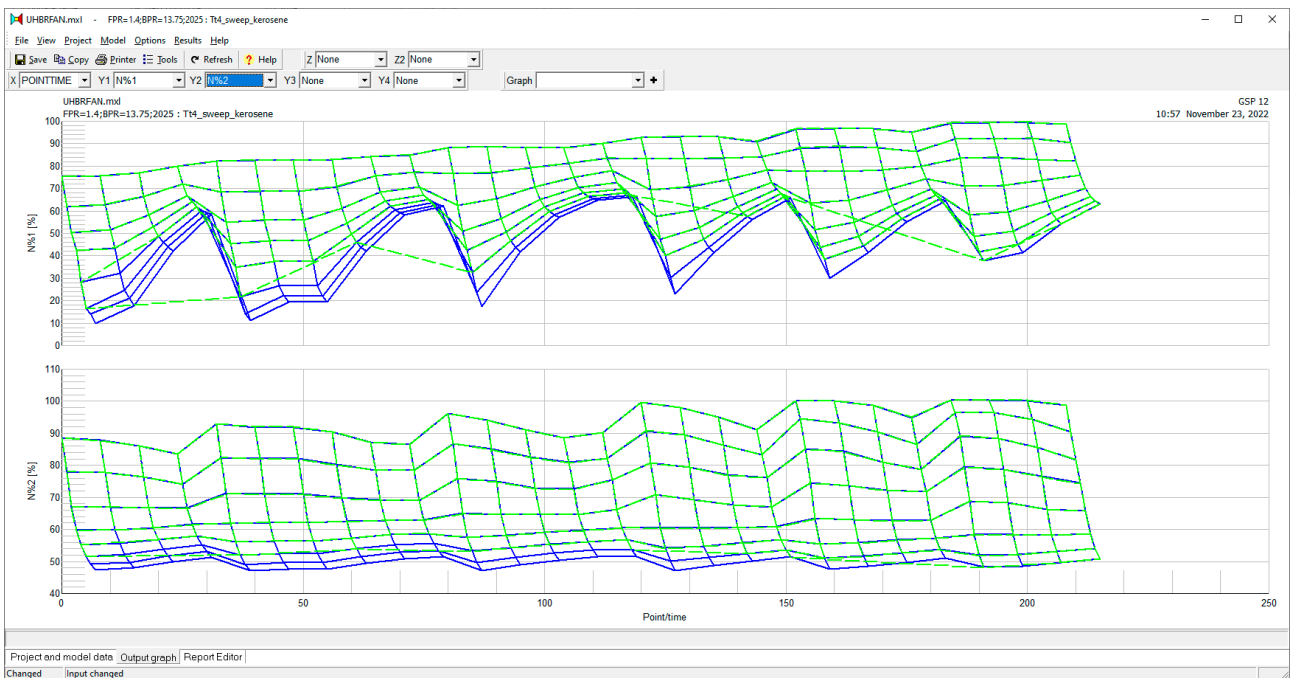


Figure 15 - Flight envelope spool speeds, hydrocarbon (solid blue) and hydrogen (dashed green)

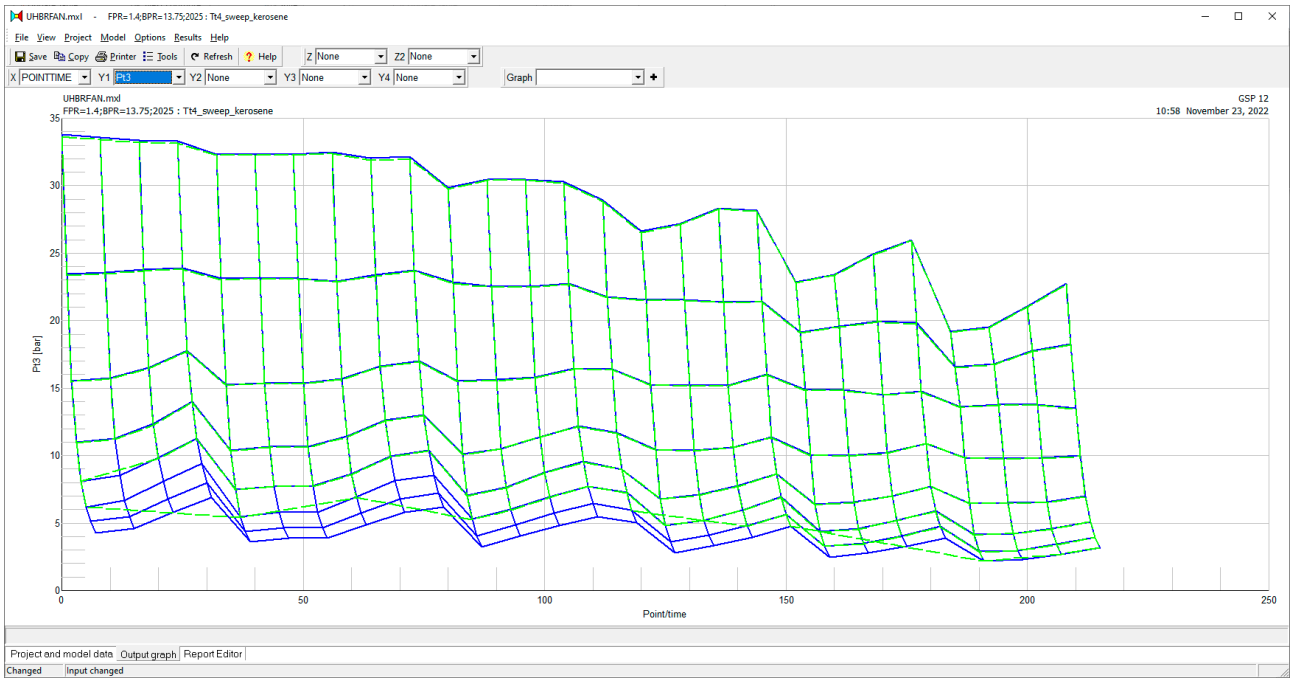


Figure 16 - Flight envelope compressor exit pressure, hydrocarbon (solid blue) and hydrogen (dashed green)

The effect of equal thrust performance causes the combustor exit temperature to lower, the effect on the LPT is shown in Figure 17. This figure shows that both entry and exit temperature are lower for a retrofit gas turbine running on Hydrogen fuel.

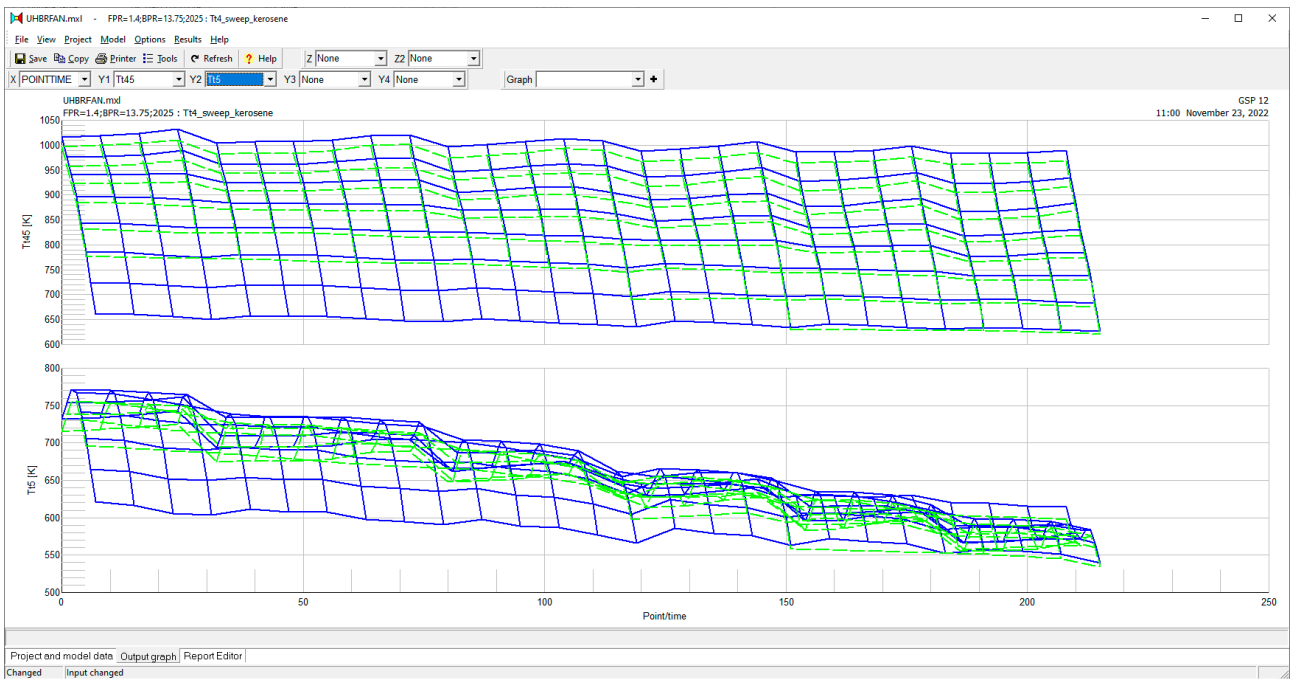


Figure 17 - Flight envelope LPT turbine temperatures, hydrocarbon (solid blue) and hydrogen (dashed green)

4 Conclusions

The analyses have shown that GSP is able to calculate the performance of UHBR turbofan engine models for the alternative fuel hydrogen. GSP facilitates the calculation of several engine designs from a single model by clever use of additional equations. The obtained results of the simulation experiments are plausible. When using net thrust (instead of fuel flow or combustor exit temperature) as power setting for the model (so that the model iterates towards the correct fuel flow) it is found that with the current settings the very low and negative thrust values do not correctly converge to a stable fuel flow. It should be investigated if more intermediate steps provide more model stability to iterate towards a valid fuel flow. Nevertheless, these low to negative net thrust values are practically not of use in real aircraft as these power settings are not required for a stable flight condition.

The simulations of chapter 2 show the optimum design point for a hydrogen design is different from a hydrocarbon jet fuel design. The optimum design for running on hydrogen for a given FPR is found at higher BPR values than for hydrocarbon jet fuel. The low pressure turbine (LPT) entry and exit temperature are higher for equivalent FPR and BPR values compared to the hydrocarbon jet fuel designs. It is concluded that pure hydrogen UHBR designs will need a higher BPR to benefit from the higher energy density of the core. A higher average low pressure turbine temperature is foreseen which may implicate alternative LPT designs (e.g. more cooling or different materials or coatings) to respect current life limits.

The simulations of chapter 3 show that for a retrofit UHBR turbofan fuelled by hydrogen, the combustor temperature is lower compared to hydrocarbon jet fuel (for equivalent thrust performance). For equivalent combustor exit temperature performance, the turbofan spool speeds (LP and HP) are higher and may exceed design limits thus negatively impact life expectancy. In the retrofit UHBR turbofan, the LPT entry and exit temperature are lower when fuelled by hydrogen compared to hydrocarbon jet fuel, while respecting all engine limits. Modifying an existing turbofan engine to be fuelled by hydrogen would be possible based on the simulations. The thrust performance can be met at lower combustor exit temperatures. This would increase the life expectancy of the LPT as the average operating temperature is lower compared to engine designs specifically designed/optimized for hydrocarbon jet fuel.

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Appendix A GSP UHBR turbofan models

Appendix A.1 Hydrocarbon 2025 reference design model



UHBRFAN.mxl

GSP 12 UHBRFAN.mxl 16:56 November 23, 2022
 MODEL DATA

=====
 Ambient / Flight conditions
 =====

Atmosphere model: ISA

Design Conditions:

 Pressure Altitude Zpdes = 10668
 Deviation from ISA temperature dTsdes = 0.00
 Static Pressure Ps0des = 0.23842
 Static temperature Ts0des = 218.81
 Density rho0des = 0.3796

Design Air speed data (Machdes was specified):

 Mach number Machdes = 0.800
 True air speed Vtdes = 237.2
 Calibrated air speed Vcdes = 139.9

Design Total free stream conditions:

 Total pressure Pt0des = 0.36344
 Total temperature Tt0des = 246.82

Design Humidity:

 Mass percent water Hum [m%] = 0.0000E+00
 Vapour volume percent Hum [v%] = 0.0000E+00
 Relative humidity Hum.Res [%] = 0.00

Off-design Conditions:

 Pressure Altitude Zp = 10668
 Deviation from ISA temperature dTs = 0.00
 Static Pressure Ps0 = 0.23842
 Static temperature Ts0 = 218.81
 Density rho0 = 0.3796

Air speed data (Mach was specified):

 Mach number Mach = 0.800
 True air speed Vt = 237.2
 Calibrated air speed Vc = 139.9

Total free stream conditions:

 Total pressure Pt0 = 0.36344
 Total temperature Tt0 = 246.82

Humidity:

 Mass percent water Hum [m%] = 0.0000E+00
 Vapour volume percent Hum [v%] = 0.0000E+00
 Relative humidity Hum.Res [%] = 0.00
 =====

Nr. 1 Component: LoopCtrl

=====
 General Data:

 Active: Checked

Loop 1 input data:

 Component: FPR_duct
 Parameter: ScheduleValue
 Start value = 1.5000E+00
 End value = 1.3000E+00
 Incr. value = -5.0000E-02
 List data:

 Title 0,1||Title 0,2
 1.5000E+00
 1.4500E+00
 1.4000E+00
 1.3500E+00
 1.3000E+00

Loop 2 input data:

 Component: Fan
 Parameter: BPRdes
 Start value = 9.000
 End value = 20.000
 Incr. value = 0.250
 List data:

 Title 0,1||Title 0,2
 9.000
 9.250
 9.500
 9.750
 10.000
 10.250
 10.500
 10.750
 11.000
 11.250
 11.500
 11.750
 12.000
 12.250
 12.500
 12.750
 13.000
 13.250
 13.500
 13.750
 14.000
 14.250
 14.500
 14.750
 15.000
 15.250
 15.500
 15.750
 16.000
 16.250
 16.500
 16.750
 17.000
 17.250
 17.500
 17.750
 18.000
 18.250
 18.500
 18.750
 19.000
 19.250
 19.500
 19.750
 20.000

 Series control input data:

Point	Break	FPR_duct FPR_duct	Fan Design BPR
1	TRUE	1.5	9.000
2		1.5	9.250
3		1.5	9.500
4		1.5	9.750
5		1.5	10.000
6		1.5	10.250
7		1.5	10.500
8		1.5	10.750

9		1.5	11.000
10		1.5	11.250
11		1.5	11.500
12		1.5	11.750
13		1.5	12.000
14		1.5	12.250
15		1.5	12.500
16		1.5	12.750
17		1.5	13.000
18	TRUE	1.45	9.000
19		1.45	9.250
20		1.45	9.500
21		1.45	9.750
22		1.45	10.000
23		1.45	10.250
24		1.45	10.500
25		1.45	10.750
26		1.45	11.000
27		1.45	11.250
28		1.45	11.500
29		1.45	11.750
30		1.45	12.000
31		1.45	12.250
32		1.45	12.500
33		1.45	12.750
34		1.45	13.000
35		1.45	13.250
36		1.45	13.500
37		1.45	13.750
38		1.45	14.000
39		1.45	14.250
40	TRUE	1.4	9.000
41		1.4	9.250
42		1.4	9.500
43		1.4	9.750
44		1.4	10.000
45		1.4	10.250
46		1.4	10.500
47		1.4	10.750
48		1.4	11.000
49		1.4	11.250
50		1.4	11.500
51		1.4	11.750
52		1.4	12.000
53		1.4	12.250
54		1.4	12.500
55		1.4	12.750
56		1.4	13.000
57		1.4	13.250
58		1.4	13.500
59		1.4	13.750
60		1.4	14.000
61		1.4	14.250
62		1.4	14.500
63		1.4	14.750
64		1.4	15.000
65		1.4	15.250
66		1.4	15.500
67		1.4	15.750
68	TRUE	1.35	9.000
69		1.35	9.250
70		1.35	9.500
71		1.35	9.750
72		1.35	10.000
73		1.35	10.250
74		1.35	10.500
75		1.35	10.750
76		1.35	11.000
77		1.35	11.250
78		1.35	11.500
79		1.35	11.750
80		1.35	12.000
81		1.35	12.250
82		1.35	12.500
83		1.35	12.750
84		1.35	13.000
85		1.35	13.250
86		1.35	13.500
87		1.35	13.750
88		1.35	14.000
89		1.35	14.250
90		1.35	14.500
91		1.35	14.750
92		1.35	15.000
93		1.35	15.250
94		1.35	15.500
95		1.35	15.750

96		1.35	16.000
97		1.35	16.250
98		1.35	16.500
99		1.35	16.750
100		1.35	17.000
101		1.35	17.250
102		1.35	17.500
103		1.35	17.750
104	TRUE	1.3	9.000
105		1.3	9.250
106		1.3	9.500
107		1.3	9.750
108		1.3	10.000
109		1.3	10.250
110		1.3	10.500
111		1.3	10.750
112		1.3	11.000
113		1.3	11.250
114		1.3	11.500
115		1.3	11.750
116		1.3	12.000
117		1.3	12.250
118		1.3	12.500
119		1.3	12.750
120		1.3	13.000
121		1.3	13.250
122		1.3	13.500
123		1.3	13.750
124		1.3	14.000
125		1.3	14.250
126		1.3	14.500
127		1.3	14.750
128		1.3	15.000
129		1.3	15.250
130		1.3	15.500
131		1.3	15.750
132		1.3	16.000
133		1.3	16.250
134		1.3	16.500
135		1.3	16.750
136		1.3	17.000
137		1.3	17.250
138		1.3	17.500
139		1.3	17.750
140		1.3	18.000
141		1.3	18.250
142		1.3	18.500
143		1.3	18.750
144		1.3	19.000
145		1.3	19.250
146		1.3	19.500
147		1.3	19.750
148		1.3	20.000

Nr. 2 Component: FPRduct_sched

General Data:

Input1 Expression result = 1.3000000000000004

Active: Checked
 Scheduled component property: Fan
 DP property: PRdesduct : Double
 Expression: FPR_duct

Nr. 3 Component: FPRcore_sched

General Data:

Input1 Expression result = 1.23499999999999988

Active: Checked
 Scheduled component property: Fan
 DP property: PRdescore : Double
 Expression: FPR_duct*0.95

Nr. 4 Component: FPRcore_sched1

General Data:

```
-----
Input1                               Expression result = 32.4969872584729131
-----
```

```
Active: Checked
Scheduled component property: HPC
DP property: PRdes : Double
Expression: OPRdes/PR_lpc/(FPR_duct*0.95)
-----
=====
```

Nr. 5 Component: DP Equation Control

General Data:

```
-----
Input1                               Name input1 = 0
-----
```

Design Point Data:

```
-----
Inputldes                             ->FN =
-----
=====
```

Nr. 6 Component: Bleed Control

```
-----
Bleed flow number                       = 1
-----
```

General Data:

```
-----
Input1                               W fraction = 0.2500
-----
```

Design Point Data:

```
-----
Inputldes                             W fraction = 0.2500
-----
=====
```

Nr. 7 Component: FPR_duct

General Data:

```
-----
Output parameter name                   : FPR_duct
Expression: 1.34
Format                                  :
Comment/Unit                             :
-----
=====
```

Nr. 8 Component: OPRdes

General Data:

```
-----
Output parameter name                   : OPRdes
Expression: 60
Format                                  :
Comment/Unit                             :
-----
=====
```

Nr. 9 Component: Inlet Station nrs.: ltOut1: 2

General Data:

```
-----
MIL standard Ram Recovery
-----
```

Design Point Data:

```
-----
ExitArea                               Aexit2 Area = 0.0000
inlet front flow cross area            Ainlet front [m²] = 0.0000
inlet exit flow cross area             Ainlet exit [m²] = 0.0000
Mass flow                               Wdes = 359.8662
Ram recovery factor                     RRdes = 1.000
-----
=====
```

Nr. 10 Component: Fan Station nrs.: ltIn1: 2 ltOut1: 24 ltOut2: 13

General Data:

```
-----
Shaft nr./suffix                               ShaftID : 1
Free State Rotor speed
Gear ratio                                     GR = 1.000
Fan drive gear box efficiency                 ETAgearbox = 1.000
Correction factor for eff. map flows         CF = 0.000
-----
```

```
-----
Design Point Data:
-----
Design bypass ratio                           BPRdes = 9.000
Rotor speed                                  Ndes [rpm] = 1500
Core side pressure ratio                     PRdesdesCore = 1.425
Duct side pressure ratio                    PRdesdesDuct = 1.500
Core side isentropic efficiency             ETAdesCore = 0.900
Duct side isentropic efficiency             ETAdesDuct = 0.940
-----
```

```
-----
Map data:
-----
Core side map text file name                 :
Map design rotor speed                     NcmapdesCore [rpm] = 1.000
Map design Beta value                      BetamapdesCore = 0.571429
Map design rotor speed                     NcmapdesDuct = 1.000
Map design Beta value                      BetamapdesDuct = 0.571429
-----
```

Nr. 11 Component: Booster Station nrs.: ltIn1: 24 ltOut1: 26

```
-----
General Data:
-----
Shaft nr./suffix                               ShaftID : 1
Free State Rotor speed
Gear ratio                                     GR = 1.000
-----
```

```
-----
Design Point Data:
-----
ExitArea                                       Aexit2 Area = 0.0000
Rotor speed                                  Ndes [rpm] = 3390
Design % rotor speed                        Npercdes [%] = 100.00
Design gear ratio                          GRdes = 1.000
Isentropic efficiency                      ETAis = 0.900
Design pressure ratio                      PRdes = 1.495
-----
```

```
-----
Map data:
-----
Map design rotor speed                     Ncmapdes = 1.000
Map Design Beta value                      Betamapdes = 0.571429
-----
```

Nr. 12 Component: HPC Station nrs.: ltIn1: 26 ltOut1: 3

```
-----
General Data:
-----
Shaft nr./suffix                               ShaftID : 2
Free State Rotor speed
Gear ratio                                     GR = 1.000
-----
```

```
-----
Design Point Data:
-----
ExitArea                                       Aexit2 Area = 0.0000
Rotor speed                                  Ndes [rpm] = 10300
Design % rotor speed                        Npercdes [%] = 100.00
Design gear ratio                          GRdes = 1.000
Isentropic efficiency                      ETAis = 0.900
Design pressure ratio                      PRdes = 28.1641
-----
```

```
-----
Map data:
-----
Map design rotor speed                     Ncmapdes = 1.000
Map Design Beta value                      Betamapdes = 0.60979
-----
```

```
-----
Compressor Bleed flows:
-----
Nr  Type  W bleed  Bleed fraction  dH fraction
1  Externally Controlled  0.000  0.0000  1
-----
```

Nr. 13 Component: Manual Fuel Control

General Data:

```
-----
Input1                               Wf = 0.784
Fuel flow                             Wf [kg/s] = 0.784
-----
```

Design Point Data:

```
-----
Input1des                             Wf = 2.4912
-----
-----
```

Nr. 14 Component: Combustor Station nrs.: ltIn1: 3 ltOut1: 4

General Data:

```
-----
User specified combustion efficiency
Combustion efficiency                 ETA = 0.9950
Burner duct cross area                A [m²] = 0.3800
-----
```

Fuel type: Jet A/A1, JP-8, Avtur

```
-----
H / C ratio                           HCrat = 1.9167
O / C ratio                             OCrat = 0.000
Off design heating value (HV) at TrefHVCpdes  LHV = 43031.000
-----
```

Design Point Data:

```
-----
ExitMach                               Aexit2 Mach = 0.258114
Design Fuel type: Jet A/A1, JP-8, Avtur
-----
```

```
-----
Design H / C ratio                     HCratdes = 1.9167
Design O / C ratio                     OCratdes = 0.000
Temp. for design lower heating value (HV) spec.TrefHVCpdes [K] = 298.15
Design Lower heating value at TrefHVCpdes    LHVdes = 43031.000
-----
```

```
-----
Design exit temperature                 Ttexit [K] = 1650.00
Design combustion efficiency            ETAdes = 0.9950
Relative total pressure loss           dPreldes = 0.0400
-----
```

Pressure Loss Data:

```
-----
User specified rel. pressure loss       Dprel = 0.0000
-----
```

Emission model: Semi-empirical ratio- or direct prediction method

```
-----
Design point emission indices [g/kg fuel] :
NOx design point emission index        EInoxdes = 28.060
CO design point emission index         EICodes = 0.520
UHC design point emission index        EIuhcdes = 0.080
Design point Smoke number              SNdes = 7.100
-----
```

Ratio NOx model (relative to design EI) used

Nr. 15 Component: HPT Station nrs.: ltIn1: 4 ltOut1: 45

General Data:

```
-----
Shaft nr./suffix                       ShaftID : 2
Free State Rotor speed
Gear ratio                               GR = 1.000
Spool inertial moment                   Ispinert [kg m²] = 0.7578
Spool mechanical efficiency             ETAm = 0.990
-----
```

Design Point Data:

```
-----
ExitArea                               Aexit2 Area = 0.0000
Rotor speed                             Ndes [rpm] = 10300
Design % rotor speed                    Npercdes [%] = 100.00
Design gear ratio                       GRdes = 1.000
Isentropic efficiency                   ETAIs = 0.880
design External power off-take          PTO [kW] = 0.00
design External torque load             TQ [N m] = 0
-----
```

Map data:

```

Map design rotor speed          Ncmapdes = 1.000
Map Design Beta value          Betamapdes = 0.864906
=====

```

```

Nr. 16 Component: LPT Station nrs.: ltIn1: 45 ltOut1: 5
=====

```

```

General Data:
-----

```

```

Shaft nr./suffix                ShaftID : 1
Free State Rotor speed
Gear ratio                       GR = 1.000
Spool inertial moment            Ispinert [kg m²] = 0.7578
Spool mechanical efficiency      ETAm = 0.990
-----

```

```

Design Point Data:
-----

```

```

ExitArea                        Aexit2 Area = 0.0000
Rotor speed                     Ndes [rpm] = 3390
Design % rotor speed            Npercdes [%] = 100.00
Design gear ratio               GRdes = 1.000
Isentropic efficiency           ETAis = 0.925
design External power off-take   PTO [kW] = 0.00
design External torque load      TQ [N m] = 0
-----

```

```

Map data:
-----

```

```

Map design rotor speed          Ncmapdes = 1.000
Map Design Beta value          Betamapdes = 0.700
=====

```

```

Nr. 17 Component: Hot core duct Station nrs.: ltIn1: 5 ltOut1: 7
=====

```

```

General Data:
-----

```

```

Design Point Data:
-----

```

```

ExitArea                        Aexit2 Area = 0.0000
Flow 1 rel. tot. pressure loss at design point dprelldes = 0.010
-----

```

```

Pressure Loss Data:
-----

```

```

Specified design rel. pressure loss only
Off-des rel. dp is corrected proportional to Wc²
=====

```

```

Nr. 18 Component: Hot exhaust nozzle Station nrs.: ltIn1: 7
=====

```

```

General Data:
-----

```

```

Velocity coefficient            CV = 0.990
Thrust coefficient              CX = 1.000
Fixed throat area nozzle
Convergent nozzle
-----

```

```

Design Point Data:
-----

```

```

ExitArea                        Aexit2 Area = 0.0000
Design Velocity coefficient      CV = 0.990
Design Thrust coefficient        CX = 1.000
Effective nozzle area           CD throat = 1.000
-----

```

```

Nr. 19 Component: Fan bypass duct Station nrs.: ltIn1: 13 ltOut1: 17
=====

```

```

General Data:
-----

```

```

Design Point Data:
-----

```

```

ExitArea                        Aexit2 Area = 0.0000
Flow 1 rel. tot. pressure loss at design point dprelldes = 0.020
-----

```

Pressure Loss Data:

```
-----
Specified design rel. pressure loss only
Off-des rel. dp is corrected proportional to Wc2
=====
```

```
Nr. 20 Component: Cold exhaust nozzle Station nrs.: ltIn1: 17
=====
```

General Data:

```
-----
Velocity coefficient                CV = 0.990
Thrust coefficient                  CX = 1.000
Fixed throat area nozzle
Convergent nozzle
=====
```

Design Point Data:

```
-----
ExitArea                            Aexit2 Area = 0.0000
Design Velocity coefficient          CV = 0.990
Design Thrust coefficient            CX = 1.000
Effective nozzle area                CD throat = 1.000
=====
```

Appendix A.2 Hydrogen 2025 design model difference

```
Nr. 1 Component: LoopCtrl
=====
```

General Data:

```
-----
Active: Checked
=====
```

Loop 1 input data:

```
-----
Component: FPR_duct
Parameter: ScheduleValue
Start value                = 1.5000E+00
End value                   = 1.3000E+00
Incr. value                 = -5.0000E-02
List data:
=====
```

```
Title 0,1||Title 0,2
          1.5000E+00
          1.4500E+00
          1.4000E+00
          1.3500E+00
          1.3000E+00
=====
```

Loop 2 input data:

```
-----
Component: Fan
Parameter: BPRdes
Start value                = 9.000
End value                   = 20.000
Incr. value                 = 0.250
List data:
=====
```

```
Title 0,1||Title 0,2
          9.000
          9.250
          9.500
          9.750
          10.000
          10.250
          10.500
          10.750
          11.000
          11.250
          11.500
          11.750
          12.000
          12.250
          12.500
          12.750
          13.000
          13.250
          13.500
          13.750
          14.000
=====
```


14.250
 14.500
 14.750
 15.000
 15.250
 15.500
 15.750
 16.000
 16.250
 16.500
 16.750
 17.000
 17.250
 17.500
 17.750
 18.000
 18.250
 18.500
 18.750
 19.000
 19.250
 19.500
 19.750
 20.000

 Series control input data:

Point	Break	FPR_duct	FPR_duct	Fan	Design BPR
1	TRUE		1.5		9.000
2			1.5		9.250
3			1.5		9.500
4			1.5		9.750
5			1.5		10.000
6			1.5		10.250
7			1.5		10.500
8			1.5		10.750
9			1.5		11.000
10			1.5		11.250
11			1.5		11.500
12			1.5		11.750
13			1.5		12.000
14			1.5		12.250
15			1.5		12.500
16			1.5		12.750
17			1.5		13.000
18			1.5		13.250
19			1.5		13.500
20			1.5		13.750
21			1.5		14.000
22	TRUE	1.45			9.000
23		1.45			9.250
24		1.45			9.500
25		1.45			9.750
26		1.45			10.000
27		1.45			10.250
28		1.45			10.500
29		1.45			10.750
30		1.45			11.000
31		1.45			11.250
32		1.45			11.500
33		1.45			11.750
34		1.45			12.000
35		1.45			12.250
36		1.45			12.500
37		1.45			12.750
38		1.45			13.000
39		1.45			13.250
40		1.45			13.500
41		1.45			13.750
42		1.45			14.000
43		1.45			14.250
44		1.45			14.500
45		1.45			14.750
46		1.45			15.000
47		1.45			15.250
48	TRUE	1.4			9.000
49		1.4			9.250
50		1.4			9.500
51		1.4			9.750
52		1.4			10.000
53		1.4			10.250
54		1.4			10.500
55		1.4			10.750
56		1.4			11.000
57		1.4			11.250
58		1.4			11.500

59		1.4	11.750
60		1.4	12.000
61		1.4	12.250
62		1.4	12.500
63		1.4	12.750
64		1.4	13.000
65		1.4	13.250
66		1.4	13.500
67		1.4	13.750
68		1.4	14.000
69		1.4	14.250
70		1.4	14.500
71		1.4	14.750
72		1.4	15.000
73		1.4	15.250
74		1.4	15.500
75		1.4	15.750
76		1.4	16.000
77		1.4	16.250
78		1.4	16.500
79		1.4	16.750
80		1.4	17.000
81	TRUE	1.35	9.000
82		1.35	9.250
83		1.35	9.500
84		1.35	9.750
85		1.35	10.000
86		1.35	10.250
87		1.35	10.500
88		1.35	10.750
89		1.35	11.000
90		1.35	11.250
91		1.35	11.500
92		1.35	11.750
93		1.35	12.000
94		1.35	12.250
95		1.35	12.500
96		1.35	12.750
97		1.35	13.000
98		1.35	13.250
99		1.35	13.500
100		1.35	13.750
101		1.35	14.000
102		1.35	14.250
103		1.35	14.500
104		1.35	14.750
105		1.35	15.000
106		1.35	15.250
107		1.35	15.500
108		1.35	15.750
109		1.35	16.000
110		1.35	16.250
111		1.35	16.500
112		1.35	16.750
113		1.35	17.000
114		1.35	17.250
115		1.35	17.500
116		1.35	17.750
117		1.35	18.000
118		1.35	18.250
119		1.35	18.500
120		1.35	18.750
121		1.35	19.000
122		1.35	19.250
123	TRUE	1.3	9.000
124		1.3	9.250
125		1.3	9.500
126		1.3	9.750
127		1.3	10.000
128		1.3	10.250
129		1.3	10.500
130		1.3	10.750
131		1.3	11.000
132		1.3	11.250
133		1.3	11.500
134		1.3	11.750
135		1.3	12.000
136		1.3	12.250
137		1.3	12.500
138		1.3	12.750
139		1.3	13.000
140		1.3	13.250
141		1.3	13.500
142		1.3	13.750
143		1.3	14.000
144		1.3	14.250
145		1.3	14.500

146	1.3	14.750
147	1.3	15.000
148	1.3	15.250
149	1.3	15.500
150	1.3	15.750
151	1.3	16.000
152	1.3	16.250
153	1.3	16.500
154	1.3	16.750
155	1.3	17.000
156	1.3	17.250
157	1.3	17.500
158	1.3	17.750
159	1.3	18.000
160	1.3	18.250
161	1.3	18.500
162	1.3	18.750
163	1.3	19.000
164	1.3	19.250
165	1.3	19.500
166	1.3	19.750
167	1.3	20.000

Nr. 14 Component: Combustor Station nrs.: ItIn1: 3 ItOut1: 4

General Data:

User specified combustion efficiency
Combustion efficiency ETA = 0.9950
Burner duct cross area A [m²] = 0.3800

Fuel type: H2 (gas)

H / C ratio HCrat = 0.000
O / C ratio OCrat = 0.000
Off design heating value (HV) at TrefHVCpdes LHV = 120000.000

Design Point Data:

ExitMach Aexit2 Mach = 0.258114
Design Fuel type: H2 (gas)

Design H / C ratio HCratdes = 0.000
Design O / C ratio OCratdes = 0.000
Temp. for design lower heating value (HV) spec.TrefHVCpdes [K] = 298.15
Design Lower heating value at TrefHVCpdes LHVdes = 120000.000

Design exit temperature Ttextit [K] = 1650.00
Design combustion efficiency ETAdes = 0.9950
Relative total pressure loss dPreldes = 0.0400

Pressure Loss Data:

User specified rel. pressure loss Dprel = 0.0000

Emission model: Semi-empirical ratio- or direct prediction method

Design point emission indices [g/kg fuel] :
NOx design point emission index EInoxdes = 28.060
CO design point emission index EICODES = 0.520
UHC design point emission index EIUHCDDES = 0.080
Design point Smoke number SNDES = 7.100

Ratio NOx model (relative to design EI) used

Appendix A.3 Retrofit 2025 turbofan model

Appendix A.3.1 Reference hydrocarbon fuel model

=====
 Ambient / Flight conditions
 =====

Atmosphere model: ISA

Design Conditions:

 Pressure Altitude Zpdes = 10000
 Deviation from ISA temperature dTsdes = 0.00
 Static Pressure Ps0des = 0.23842
 Static temperature Ts0des = 218.81
 Density rho0des = 0.4127

Design Air speed data (Machdes was specified):

 Mach number Machdes = 0.800
 True air speed Vtdes = 237.2
 Calibrated air speed Vcdes = 139.9

Design Total free stream conditions:

 Total pressure Pt0des = 0.36344
 Total temperature Tt0des = 246.82

Design Humidity:

 Mass percent water Hum [m%] = 0.0000E+00
 Vapour volume percent Hum [v%] = 0.0000E+00
 Relative humidity Hum.Res [%] = 0.00

Off-design Conditions:

 Pressure Altitude Zp = 10000
 Deviation from ISA temperature dTs = 0.00
 Static Pressure Ps0 = 0.26436
 Static temperature Ts0 = 223.15
 Density rho0 = 0.4127

Air speed data (Mach was specified):

 Mach number Mach = 0.800
 True air speed Vt = 239.6
 Calibrated air speed Vc = 147.0

Total free stream conditions:

 Total pressure Pt0 = 0.40298
 Total temperature Tt0 = 251.71

Humidity:

 Mass percent water Hum [m%] = 0.0000E+00
 Vapour volume percent Hum [v%] = 0.0000E+00
 Relative humidity Hum.Res [%] = 0.00

Flight conditions transient input data:

Pnt/Time	Zp	dTs	Ps	Ts	Mach	Vt	Vc	Type
0.000	0	0.00	1.01325	288.15	0.000	0.0	0.0	ISA
1.000	0	0.00	1.01325	288.15	0.000	0.0	0.0	ISA
2.000	0	0.00	1.01325	288.15	0.000	0.0	0.0	ISA
3.000	0	0.00	1.01325	288.15	0.000	0.0	0.0	ISA
4.000	0	0.00	1.01325	288.15	0.000	0.0	0.0	ISA
5.000	0	0.00	1.01325	288.15	0.000	0.0	0.0	ISA
6.000	0	0.00	1.01325	288.15	0.000	0.0	0.0	ISA
7.000	0	0.00	1.01325	288.15	0.000	0.0	0.0	ISA
8.000	0	0.00	1.01325	288.15	0.200	68.1	68.1	ISA
9.000	0	0.00	1.01325	288.15	0.200	68.1	68.1	ISA
10.000	0	0.00	1.01325	288.15	0.200	68.1	68.1	ISA
11.000	0	0.00	1.01325	288.15	0.200	68.1	68.1	ISA
12.000	0	0.00	1.01325	288.15	0.200	68.1	68.1	ISA
13.000	0	0.00	1.01325	288.15	0.200	68.1	68.1	ISA
14.000	0	0.00	1.01325	288.15	0.200	68.1	68.1	ISA
15.000	0	0.00	1.01325	288.15	0.200	68.1	68.1	ISA
16.000	0	0.00	1.01325	288.15	0.400	136.1	136.1	ISA
17.000	0	0.00	1.01325	288.15	0.400	136.1	136.1	ISA
18.000	0	0.00	1.01325	288.15	0.400	136.1	136.1	ISA
19.000	0	0.00	1.01325	288.15	0.400	136.1	136.1	ISA

194.000	10000	0.00	0.26436	223.15	0.400	119.8	70.6	ISA
195.000	10000	0.00	0.26436	223.15	0.400	119.8	70.6	ISA
196.000	10000	0.00	0.26436	223.15	0.400	119.8	70.6	ISA
197.000	10000	0.00	0.26436	223.15	0.400	119.8	70.6	ISA
198.000	10000	0.00	0.26436	223.15	0.400	119.8	70.6	ISA
199.000	10000	0.00	0.26436	223.15	0.400	119.8	70.6	ISA
200.000	10000	0.00	0.26436	223.15	0.600	179.7	107.7	ISA
201.000	10000	0.00	0.26436	223.15	0.600	179.7	107.7	ISA
202.000	10000	0.00	0.26436	223.15	0.600	179.7	107.7	ISA
203.000	10000	0.00	0.26436	223.15	0.600	179.7	107.7	ISA
204.000	10000	0.00	0.26436	223.15	0.600	179.7	107.7	ISA
205.000	10000	0.00	0.26436	223.15	0.600	179.7	107.7	ISA
206.000	10000	0.00	0.26436	223.15	0.600	179.7	107.7	ISA
207.000	10000	0.00	0.26436	223.15	0.600	179.7	107.7	ISA
208.000	10000	0.00	0.26436	223.15	0.800	239.6	147.0	ISA
209.000	10000	0.00	0.26436	223.15	0.800	239.6	147.0	ISA
210.000	10000	0.00	0.26436	223.15	0.800	239.6	147.0	ISA
211.000	10000	0.00	0.26436	223.15	0.800	239.6	147.0	ISA
212.000	10000	0.00	0.26436	223.15	0.800	239.6	147.0	ISA
213.000	10000	0.00	0.26436	223.15	0.800	239.6	147.0	ISA
214.000	10000	0.00	0.26436	223.15	0.800	239.6	147.0	ISA
215.000	10000	0.00	0.26436	223.15	0.800	239.6	147.0	ISA

Nr. 1 Component: Bleed Control

```

=====
Bleed flow number = 1
General Data:
-----
Input1 W fraction = 0.2500
-----
Design Point Data:
-----
Input1des W fraction = 0.2500
=====

```

Nr. 2 Component: OperEnvSched

```

=====
General Data:
-----
-----
Design Point Data:
-----
=====

```

Nr. 3 Component: Inlet Station nrs.: ltOut1: 2

```

=====
General Data:
-----
MIL standard Ram Recovery
-----
Design Point Data:
-----
ExitArea Aexit2 Area = 0.0000
inlet front flow cross area Ainlet front [m²] = 0.0000
inlet exit flow cross area Ainlet exit [m²] = 0.0000
Mass flow Wdes = 626.6965
Ram recovery factor RRdes = 1.000
=====

```

Nr. 4 Component: Fan Station nrs.: ltIn1: 2 ltOut1: 24 ltOut2: 13

```

=====
General Data:
-----
Shaft nr./suffix ShaftID : 1
Free State Rotor speed
Gear ratio GR = 1.000
Fan drive gear box efficiency ETAgearbox = 1.000
Correction factor for eff. map flows CF = 0.000
-----
Design Point Data:
-----
Design bypass ratio BPRdes = 13.750
Rotor speed Ndes [rpm] = 1500
Core side pressure ratio PRdesdesCore = 1.330

```

Duct side pressure ratio PRdesdesDuct = 1.400
 Core side isentropic efficiency ETAdesCore = 0.900
 Duct side isentropic efficiency ETAdesDuct = 0.940

 Map data:

Core side map text file name :
 Map design rotor speed NcmapdesCore [rpm] = 1.000
 Map design Beta value BetamapdesCore = 0.571429
 Map design rotor speed NcmapdesDuct = 1.000
 Map design Beta value BetamapdesDuct = 0.571429

Nr. 5 Component: Booster Station nrs.: ltIn1: 24 ltOut1: 26
 =====

General Data:

Shaft nr./suffix ShaftID : 1
 Free State Rotor speed
 Gear ratio GR = 1.000

Design Point Data:

ExitArea Aexit2 Area = 0.0000
 Rotor speed Ndes [rpm] = 3390
 Design % rotor speed Npercdes [%] = 100.00
 Design gear ratio GRdes = 1.000
 Isentropic efficiency ETAis = 0.900
 Design pressure ratio PRdes = 1.495

Map data:

Map design rotor speed Ncmapdes = 1.000
 Map Design Beta value Betamapdes = 0.571429

Nr. 6 Component: HPC Station nrs.: ltIn1: 26 ltOut1: 3
 =====

General Data:

Shaft nr./suffix ShaftID : 2
 Free State Rotor speed
 Gear ratio GR = 1.000

Design Point Data:

ExitArea Aexit2 Area = 0.0000
 Rotor speed Ndes [rpm] = 10300
 Design % rotor speed Npercdes [%] = 100.00
 Design gear ratio GRdes = 1.000
 Isentropic efficiency ETAis = 0.900
 Design pressure ratio PRdes = 30.1758

Map data:

Map design rotor speed Ncmapdes = 1.000
 Map Design Beta value Betamapdes = 0.60979

Compressor Bleed flows:

Nr	Type	W bleed	Bleed fraction	dH fraction	
1	Externally Controlled		0.000	0.0000	1

=====

Nr. 7 Component: Manual Fuel Control
 =====

General Data:

Input1 Ttexit = 950.00
 Exit temp. Ttexit [K] = 950.00

Design Point Data:

Inputldes Ttexit = 2.49

Series control input data:

```
-----  
Point  Ttexit  
0      1650.00  
1      1550.00  
2      1450.00  
3      1350.00  
4      1250.00  
5      1150.00  
6      1050.00  
7      950.00  
8      1650.00  
9      1550.00  
10     1450.00  
11     1350.00  
12     1250.00  
13     1150.00  
14     1050.00  
15     950.00  
16     1650.00  
17     1550.00  
18     1450.00  
19     1350.00  
20     1250.00  
21     1150.00  
22     1050.00  
23     950.00  
24     1650.00  
25     1550.00  
26     1450.00  
27     1350.00  
28     1250.00  
29     1150.00  
30     1050.00  
31     950.00  
32     1650.00  
33     1550.00  
34     1450.00  
35     1350.00  
36     1250.00  
37     1150.00  
38     1050.00  
39     950.00  
40     1650.00  
41     1550.00  
42     1450.00  
43     1350.00  
44     1250.00  
45     1150.00  
46     1050.00  
47     950.00  
48     1650.00  
49     1550.00  
50     1450.00  
51     1350.00  
52     1250.00  
53     1150.00  
54     1050.00  
55     950.00  
56     1650.00  
57     1550.00  
58     1450.00  
59     1350.00  
60     1250.00  
61     1150.00  
62     1050.00  
63     950.00  
64     1650.00  
65     1550.00  
66     1450.00  
67     1350.00  
68     1250.00  
69     1150.00  
70     1050.00  
71     950.00  
72     1650.00  
73     1550.00  
74     1450.00  
75     1350.00  
76     1250.00  
77     1150.00  
78     1050.00  
79     950.00  
80     1650.00  
81     1550.00  
82     1450.00
```

83	1350.00
84	1250.00
85	1150.00
86	1050.00
87	950.00
88	1650.00
89	1550.00
90	1450.00
91	1350.00
92	1250.00
93	1150.00
94	1050.00
95	950.00
96	1650.00
97	1550.00
98	1450.00
99	1350.00
100	1250.00
101	1150.00
102	1050.00
103	950.00
104	1650.00
105	1550.00
106	1450.00
107	1350.00
108	1250.00
109	1150.00
110	1050.00
111	950.00
112	1650.00
113	1550.00
114	1450.00
115	1350.00
116	1250.00
117	1150.00
118	1050.00
119	950.00
120	1650.00
121	1550.00
122	1450.00
123	1350.00
124	1250.00
125	1150.00
126	1050.00
127	950.00
128	1650.00
129	1550.00
130	1450.00
131	1350.00
132	1250.00
133	1150.00
134	1050.00
135	950.00
136	1650.00
137	1550.00
138	1450.00
139	1350.00
140	1250.00
141	1150.00
142	1050.00
143	950.00
144	1650.00
145	1550.00
146	1450.00
147	1350.00
148	1250.00
149	1150.00
150	1050.00
151	950.00
152	1650.00
153	1550.00
154	1450.00
155	1350.00
156	1250.00
157	1150.00
158	1050.00
159	950.00
160	1650.00
161	1550.00
162	1450.00
163	1350.00
164	1250.00
165	1150.00
166	1050.00
167	950.00
168	1650.00
169	1550.00


```

Design point emission indices [g/kg fuel] :
NOx design point emission index      EInoxdes = 28.060
CO design point emission index        EICodes = 0.520
UHC design point emission index       EIuhcdes = 0.080
Design point Smoke number              SNdes = 7.100

```

Ratio NOx model (relative to design EI) used

Nr. 9 Component: HPT Station nrs.: ltIn1: 4 ltOut1: 45

General Data:

```

-----
Shaft nr./suffix                      ShaftID : 2
Free State Rotor speed
Gear ratio                             GR = 1.000
Spool inertial moment                   Ispinert [kg m²] = 0.7578
Spool mechanical efficiency              ETAm = 0.990
-----

```

Design Point Data:

```

-----
ExitArea                               Aexit2 Area = 0.0000
Rotor speed                             Ndes [rpm] = 10300
Design % rotor speed                     Npercdes [%] = 100.00
Design gear ratio                         GRdes = 1.000
Isentropic efficiency                    ETAis = 0.880
design External power off-take            PTO [kW] = 0.00
design External torque load               TQ [N m] = 0
-----

```

Map data:

```

-----
Map design rotor speed                  Ncmapdes = 1.000
Map Design Beta value                   Betamapdes = 0.864906
-----

```

Nr. 10 Component: LPT Station nrs.: ltIn1: 45 ltOut1: 5

General Data:

```

-----
Shaft nr./suffix                      ShaftID : 1
Free State Rotor speed
Gear ratio                             GR = 1.000
Spool inertial moment                   Ispinert [kg m²] = 0.7578
Spool mechanical efficiency              ETAm = 0.990
-----

```

Design Point Data:

```

-----
ExitArea                               Aexit2 Area = 0.0000
Rotor speed                             Ndes [rpm] = 3390
Design % rotor speed                     Npercdes [%] = 100.00
Design gear ratio                         GRdes = 1.000
Isentropic efficiency                    ETAis = 0.925
design External power off-take            PTO [kW] = 0.00
design External torque load               TQ [N m] = 0
-----

```

Map data:

```

-----
Map design rotor speed                  Ncmapdes = 1.000
Map Design Beta value                   Betamapdes = 0.700
-----

```

Nr. 11 Component: Hot core duct Station nrs.: ltIn1: 5 ltOut1: 7

General Data:

Design Point Data:

```

-----
ExitArea                               Aexit2 Area = 0.0000
Flow 1 rel. tot. pressure loss at design point dprelldes = 0.010
-----

```

Pressure Loss Data:

```

-----
Specified design rel. pressure loss only
Off-des rel. dp is corrected proportional to Wc²
-----

```

```

Nr. 12 Component: Hot exhaust nozzle Station nrs.: ltIn1: 7
=====
General Data:
-----
Velocity coefficient                CV = 0.990
Thrust coefficient                 CX = 1.000
Fixed throat area nozzle
Convergent nozzle
-----

Design Point Data:
-----
ExitArea                          Aexit2 Area = 0.0000
Design Velocity coefficient        CV = 0.990
Design Thrust coefficient         CX = 1.000
Effective nozzle area             CD throat = 1.000
-----

```

```

Nr. 13 Component: Fan bypass duct Station nrs.: ltIn1: 13 ltOut1: 17
=====
General Data:
-----

Design Point Data:
-----
ExitArea                          Aexit2 Area = 0.0000
Flow 1 rel. tot. pressure loss at design point  dprelldes = 0.020
-----

Pressure Loss Data:
-----
Specified design rel. pressure loss only
Off-des rel. dp is corrected proportional to Wc²
-----

```

```

Nr. 14 Component: Cold exhaust nozzle Station nrs.: ltIn1: 17
=====
General Data:
-----
Velocity coefficient                CV = 0.990
Thrust coefficient                 CX = 1.000
Fixed throat area nozzle
Convergent nozzle
-----

Design Point Data:
-----
ExitArea                          Aexit2 Area = 0.0000
Design Velocity coefficient        CV = 0.990
Design Thrust coefficient         CX = 1.000
Effective nozzle area             CD throat = 1.000
-----

```

Appendix A.3.2 Combustor exit specified

Difference to Appendix A.3.1

```

Nr. 8 Component: Combustor Station nrs.: ltIn1: 3 ltOut1: 4
=====
General Data:
-----
User specified combustion efficiency
Combustion efficiency              ETA = 0.9950
Burner duct cross area            A [m²] = 0.3800

Fuel type: H2 (gas)

H / C ratio                       HCrat = 0.000
O / C ratio                       OCrat = 0.000
Off design heating value (HV) at TrefHVCpdes  LHV = 120000.000
-----

```

Appendix A.3.3 Thrust specified

Difference to Appendix A.3.2

Nr. 3 Component: Thrust Control

=====

General Data:

Input1 FN =

Design Point Data:

Inputldes Name input1 = 0

Series control input data:

Point	FN
0	179.373
1	111.980
2	66.877
3	42.704
4	30.074
5	21.869
6	15.651
7	10.664
8	120.225
9	68.986
10	36.195
11	20.091
12	12.080
13	7.109
14	3.817
15	1.449
16	80.437
17	42.177
18	19.518
19	8.398
20	2.820
21	-0.653
22	-2.908
23	-4.455
24	53.463
25	23.693
26	7.735
27	-0.380
28	-5.278
29	-8.156
30	-9.996
31	-11.194
32	179.977
33	118.061
34	69.462
35	42.890
36	28.219
37	19.880
38	14.340
39	9.887
40	127.482
41	77.597
42	40.653
43	22.295
44	12.431
45	7.250
46	4.080
47	1.865
48	127.186
49	77.413
50	40.529
51	22.215
52	12.373
53	7.201
54	4.043
55	1.835
56	90.370
57	49.830
58	23.515
59	11.071
60	4.188
61	0.663
62	-1.576

63	-3.049
64	61.264
65	31.748
66	11.935
67	2.370
68	-2.838
69	-5.834
70	-7.662
71	-8.809
72	55.138
73	28.261
74	9.355
75	0.137
76	-4.831
77	-7.684
78	-9.397
79	-10.498
80	120.153
81	82.309
82	44.926
83	22.362
84	11.661
85	6.563
86	3.519
87	1.533
88	94.020
89	58.488
90	29.920
91	13.304
92	5.556
93	1.753
94	-0.501
95	-1.925
96	67.568
97	39.364
98	17.355
99	5.491
100	-0.224
101	-3.503
102	-5.354
103	-6.503
104	53.232
105	29.752
106	11.834
107	1.317
108	-3.942
109	-6.931
110	-8.689
111	-9.753
112	51.302
113	29.641
114	14.210
115	2.435
116	-3.178
117	-6.132
118	-7.968
119	-9.037
120	107.373
121	80.279
122	48.261
123	25.554
124	12.184
125	6.012
126	3.043
127	1.239
128	90.141
129	63.645
130	36.071
131	17.218
132	7.431
133	2.671
134	0.366
135	-1.038
136	71.625
137	44.643
138	23.117
139	9.104
140	2.003
141	-1.532
142	-3.486
143	-4.628
144	52.185
145	31.121
146	15.417
147	3.491
148	-2.333
149	-5.367

150	-7.209
151	-8.277
152	91.817
153	71.860
154	49.924
155	26.789
156	12.203
157	5.716
158	2.702
159	0.989
160	82.337
161	63.446
162	41.660
163	21.147
164	9.060
165	3.597
166	1.066
167	-0.346
168	68.568
169	48.112
170	27.969
171	13.347
172	4.231
173	0.179
174	-1.976
175	-3.138
176	56.010
177	34.567
178	19.282
179	8.429
180	0.664
181	-2.941
182	-4.815
183	-5.913
184	75.891
185	61.757
186	46.673
187	28.750
188	13.839
189	5.898
190	2.402
191	0.800
192	72.144
193	57.846
194	43.340
195	25.464
196	12.014
197	4.835
198	1.634
199	0.202
200	62.141
201	47.705
202	31.432
203	17.404
204	6.758
205	1.623
206	-0.727
207	-1.957
208	54.403
209	37.827
210	21.883
211	11.472
212	3.405
213	-0.839
214	-2.901
215	-4.046



Dedicated to innovation in aerospace

Royal NLR - Netherlands Aerospace Centre

NLR operates as an objective and independent research centre, working with its partners towards a better world tomorrow. As part of that, NLR offers innovative solutions and technical expertise, creating a strong competitive position for the commercial sector.

NLR has been a centre of expertise for over a century now, with a deep-seated desire to keep innovating. It is an organisation that works to achieve sustainable, safe, efficient and effective aerospace operations.

The combination of in-depth insights into customers' needs, multidisciplinary expertise and state-of-the-art research facilities makes rapid innovation possible. Both domestically and abroad, NLR plays a pivotal role between science, the commercial sector and governmental authorities, bridging the gap between fundamental research and practical applications. Additionally, NLR is one of the large technological institutes (GTIs) that have been collaborating over a decade in the Netherlands on applied research united in the TO2 federation.

From its main offices in Amsterdam and Marknesse plus two satellite offices, NLR helps to create a safe and sustainable society. It works with partners on numerous programmes in both civil aviation and defence, including work on complex composite structures for commercial aircraft and on goal-oriented use of the F-35 fighter. Additionally, NLR helps to achieve both Dutch and European goals and climate objectives in line with the Luchtvaartnota (Aviation Policy Document), the European Green Deal and Flightpath 2050, and by participating in programs such as Clean Sky and SESAR.

For more information visit: www.nlr.org

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